

# Kinetics of fatty acid ketonization in liquid phase with anatase and rutile

## TiO<sub>2</sub> catalysts

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### Abstract

Catalytic ketonization of carboxylic acids is promising for the synthesis of renewable products. Despite its potential, fatty acid ketonization and its kinetics in the liquid phase are less investigated. This work encompasses kinetic evaluation of two TiO<sub>2</sub> catalysts (anatase and rutile) for C-C coupling of C<sub>12</sub>-C<sub>18</sub> fatty acids in inert dodecane solvent. The rutile catalyst, with higher Lewis acid density, showed higher intrinsic activity and more favourable activation energy barriers. Unfortunately, this material suffers from stronger product inhibition by ketone, water and carbon dioxide compared to anatase. Langmuir-Hinshelwood kinetic models were developed and validated against the experimental data, supporting that C-C coupling of adsorbed species is rate determining in the ketonization mechanism. The Lewis acid site density and distance between active Ti species at the surface were invoked to explain the activity patterns. The impacts of substrate chain length, solvent and liquid phase purging on the ketonization kinetics were investigated, showcasing potential for future improvements.

### 1. Introduction

Ketonization of carboxylic acids is a unique C-C coupling reaction that converts two carboxylic acid molecules into an internal ketone with increased chain length, and water and carbon dioxide side products.[1] Via this chemical pathway, carboxylic acids present in lignocellulose and oleochemical biomass can be valorised into renewable fuels and chemicals (or their intermediates).[2] Indeed, pyrolysis bio-oil and its model compounds, typically C<sub>2</sub>-C<sub>4</sub> carboxylic acids, have been studied extensively as substrates for this C-C coupling reaction.[3-5] In contrast, ketonization studies utilizing vegetable oils and animal fats (C<sub>12</sub>-C<sub>18</sub> fatty acids) are far less prevalent in literature, even though their specific chain length, limited chemical functionality and large scale availability should make them attractive substrates to synthesize renewable C<sub>23</sub>-C<sub>35</sub> ketone bio-waxes.[6] Besides direct use as (wax type) end products[7], consecutive hydrodeoxygenation and hydro-isomerisation of these bio-based compounds yields hydrocarbon wax and lubricant products.[8]

Ketonization of carboxylic acids has been the subject of critical review.[2, 9-11] From the large array of (heterogeneous) catalysts employed, metal oxides, and in particular amphoteric TiO<sub>2</sub>, CeO<sub>2</sub>, ZrO<sub>2</sub>, are presented as

most suitable due to a combination of high activity, selectivity (and stability) for this reaction. Latest literature indicates that their active surface sites, coordinatively unsaturated Lewis acid-base  $M^{x+}-O^{y-}$  pairs, catalyse the ketonization reaction via a  $\beta$ -ketoacid mechanism.[12-16] Several reports have been published on the kinetics of catalytic ketonization, almost exclusively when starting from  $C_2$ - $C_4$  acids in gas phase processes.

For instance, the C-C coupling of acetic acid with a bifunctional Ru/TiO<sub>2</sub> catalyst has been described by a power law equation, revealing a positive observed substrate reaction order value of 1.6.[17] Multiple groups have reported an asymptotic relationship between the reaction rate and initial carboxylic acid concentration, resulting in fractional observed substrate orders, signalling the transition from a second[18] or first[19] to zero order reaction and saturation of the catalytic sites on the surface.[20, 21] Oppositely, negative partial orders were found for all three reaction products, i.e. for acetone (-0.4), CO<sub>2</sub> (-0.2) and H<sub>2</sub>O (-0.1), indicating the occurrence of product inhibition by competing for adsorption on the catalytic sites. The C-C coupling was proposed as rate determining elementary step in the ketonization mechanism. While suppression of the reaction rate by the ketonization products was not permanent in this particular case, others have observed irreversible deactivation by H<sub>2</sub>O when using Ce<sub>0.7</sub>Ti<sub>0.3</sub>O<sub>x</sub>. [22] This was ascribed to competitive surface adsorption, hydrolysis of reaction intermediates or disintegration of the active material under hydrothermal conditions. Depending on the specific substrate, catalyst and reactor system under investigation, relevant literature has not only shown different orders and strength of substrate adsorption and product inhibition, but also their ketonization temperature dependency (adsorption enthalpy).[13, 23, 24]

Related to this, the influence of the feedstock chain length on the substrate-surface interaction, and therefore ketonization kinetics, has been studied in detail. As a rule, the reaction is slower when starting from longer carboxylic acids. For ketonization of  $C_2$ - $C_4$  carboxylic acids on Ru/TiO<sub>2</sub>[25] and HZSM-5[26] catalysts, this has been linked to the difference in contribution of the adsorption entropy. For instance, a value of -198 J/mol.K was calculated for acetic acid on Ru/TiO<sub>2</sub>, while this increased to -178 J/mol.K for butyric acid. This relationship was also found for other kinetic and thermodynamic parameters such as the true activation energy, activation entropy and activation enthalpy. In contrast, no difference was found in the adsorption enthalpy values when varying the ketonization feedstock. These findings imply that the substrate-surface interaction is not governed by the alkyl tail, but rather by adsorption of the polar acid group. Additionally, it is clear that the transition state requires more space in the immediate surroundings of the active sites during C-C bond formation of carboxylic acid molecules with a higher carbon number. As a result, this steric hindrance slows down the rate determining step for longer carboxylic acids, increasing the energy demand.

To describe the rate determining step of  $C_2$ - $C_4$  gas-phase ketonization, Langmuir-Hinshelwood (LH) kinetic models have been proposed the most. Depending on the specific conditions, these may include or exclude inhibition by one of the reaction products, while adsorption of all relevant species is generally described by competition for the same catalytic site.[2] The few existing liquid phase ketonization studies have mainly focused on C-C coupling of acetic acid in aqueous reaction media. To maintain liquid phase conditions, very high reaction pressures (up to 190 bar) have been reported when operating at a high ketonization temperature (340°C).[27] In contrast, Ru/TiO<sub>2</sub>, TiO<sub>2</sub>/C and Ru/TiO<sub>2</sub>/C catalysts have been used at 180 °C in various solvents such as hexane, N-Methyl-2-pyrrolidone and water.[28] The highest ketonization activity was achieved with Ru/TiO<sub>2</sub>/C in the organic media, reportedly due to the hydrophobic nature of this support material limiting the amount of water inhibition. Related to the latter, others have also observed increased activity and/or stability of more hydrophobic ketonization catalysts such as HF treated

TiO<sub>2</sub>[29] and ZrO<sub>2</sub>/C[30] when using water as ketonization solvent. The most striking example was reported by Aranda-Pérez *et al.* where a 5% Ru/TiO<sub>2</sub> catalyst was only active for aqueous phase acetic acid ketonization when the TiO<sub>2</sub> crystal phase was rutile.[31] Both anatase and P25 (anatase-rutile mixture) TiO<sub>2</sub> phases were inactive, in contrast to the experiments carried out in hexane. Additionally, catalyst phase changes may occur due to the hydrothermal ketonization conditions, as has been shown for amorphous La<sub>x</sub>Zr<sub>y</sub>O<sub>z</sub> catalysts undergoing crystallization.[32] Interestingly, the reaction of C<sub>2</sub> carboxylic acid has been studied theoretically in both gas and liquid aqueous phase using a ZrO<sub>2</sub> catalyst.[33] The ketonization kinetics in water were best described by an Eley-Rideal (ER) mechanism, with a lower ketonization rate compared to the gas phase. In this reaction medium, the amount of available acid-base pairs for ketonization was reduced significantly as a consequence of competitive adsorption by H<sub>2</sub>O, which can furthermore also hydroxylate the active sites and take part in proton transfer reactions during the elementary steps of the ketonization mechanism (Grotthuss mechanism). In conclusion, the reaction environment surrounding the active surface is noticeably more complicated for liquid phase ketonization reactions. Detailed investigation of the liquid phase reaction kinetics for C<sub>12</sub>-C<sub>18</sub> carboxylic acid using heterogenous catalysts is currently missing in this research field. It must be noted that the kinetics of liquid phase C-C coupling of stearic acid, in dodecane solvent and absence of catalyst addition, has been published.[34] The observed catalytic ketonization activity was assigned to the stainless steel reactor wall in this particular case. Shorter reactions (3 hours) starting from low fatty acid concentrations (0.15 M) resulted in high selectivity to the 18-pentatriacontanone product. However, fatty acid decarboxylation became the dominant reaction pathway for longer reactions (96 hours) at higher temperatures and substrate loadings (1.75 M), considerably reducing the ketonization selectivity. Low conversion (20-30%) and selectivity (18-22%) values have also been reported for ketonization of stearic acid when using ZrO<sub>2</sub> catalysts in dodecane in hydrogen atmosphere (40 bar) at 260 °C.[35]

This concise overview reveals some of the recent progress made to better understand the mechanism and kinetics of short-chain carboxylic acid ketonization in the gas phase. However, no kinetic study has been performed on the (liquid phase) catalytic ketonization of fatty acids, to the best of our knowledge. Evidently, this information is required for the design and development of future ketonization biorefinery processes for the synthesis of bio-based waxes and derivatives. As a result, the key goal of this work is to describe and model the liquid phase kinetics of fatty acid ketonization. Hereto, the activity of two commercial TiO<sub>2</sub> catalysts (anatase (A) and rutile (R)) is investigated kinetically in a (semi-)batch reactor in dodecane solvent. These reaction data are used to develop a kinetic model, describing the reaction of the catalysis, which is linked to the physicochemical surface properties of the catalysts. Furthermore, the influence of substrate properties (such as chain length), reactor mode and operating conditions are explored to test and validate the kinetic model. Possible deactivation effects by ketonization products are studied explicitly. Finally, this study compares these results to earlier developed kinetic concepts derived from the short-chain gas phase studies, and discusses both similarities and differences.

## **2. Experimental**

### **2.1 Chemicals & materials**

#### **2.1.1 Substrates**

The following fatty acid substrates were used in this study: lauric acid (98%, Sigma Aldrich), myristic acid (98%, Sigma Aldrich), palmitic acid (98%, Acros Organics), stearic acid (97%, Acros Organics) and arachidic acid (99%, Fisher Scientific).

### **2.1.2 Products**

All ketone products were purchased from TCI Europe: laurone (12-tricosanone, 95%), myristone (14-heptacosanone, 95%), palmitone (16-hentriacontanone, 95%) and stearone (18-pentatriacontanone, 95%).

### **2.1.3 Catalysts**

The commercial TiO<sub>2</sub> catalysts under investigation were kindly provided by Venator (Hombikat M211, anatase (A) and Hombikat Mikrorutil, rutile (R)).

### **2.1.4 Other chemicals**

The eicosane standard (99%), n-dodecane reaction solvent (99%) and chloroform analysis solvent (HPLC grade) were purchased from Acros Organics. The N-methyl-N-(trimethylsilyl)trifluoroacetamide (MSTFA, 98.5%) derivatization agent for trimethylsilylation was purchased from Sigma Aldrich.

## **2.2 Catalyst characterization**

### **2.2.1 X-ray diffraction**

A Stadi P Combi diffractometer instrument (STOE), capable of high-throughput analysis, was used to perform the powder X-ray diffraction measurements. The data were collected in transmission mode (CuK $\alpha$ 1 ( $\lambda$ =1.54 Å) radiation, Ge (111) monochromator) using an image plate position sensitive detector. The applied scanning range for 2 $\theta$  was 5-60°.

### **2.2.2 Scanning electron microscopy**

Scanning electron microscopy images were collected by a JSM-6010 JV microscope (JEOL) at 10 kV accelerating voltage. Prior to imaging, a gold coating was applied to the catalyst materials using JSC-1300 sputter equipment (JEOL).

### **2.2.3 Nitrogen physisorption**

The catalyst powders were first pre-treated in a constant N<sub>2</sub>-flow at 300 °C for 5 h. Afterwards, the N<sub>2</sub> isotherms were recorded at -196 °C by a Tristar II 3020 instrument (Micromeritics). Catalyst surface areas and pore sizes were quantified by BET and BJH analysis, respectively.

### **2.2.4 Temperature-programmed desorption**

First, pellets (250-500  $\mu$ m) were made from the original TiO<sub>2</sub> powder samples and loaded into a quartz tube inside a customized plug flow fixed bed measurement system. Quartz wool was used to keep the catalyst sample in place, while pelletizing ensures gas plug flow at constant pressure while minimizing the risk of clogging, tunnelling and pressure build-up and losses as would be the risk for the powder samples. For ammonia TPD, the pre-treatment

step consisted of heating at 5 °C/min to 400 °C in He. This temperature was maintained for 1 h, after which the catalyst sample was cooled to 150 °C. Then, NH<sub>3</sub> was allowed to adsorb for 30 min, followed by additional flushing with He for 30 minutes to remove physisorbed NH<sub>3</sub>. Desorption of gasses (m/z=16 for NH<sub>3</sub>) was analysed from 150 °C to 800 °C (10 °C/min ramp). For CO<sub>2</sub> (m/z= 44), the experimental procedure was identical, except lowering the adsorption temperature to 50 °C. All datapoints were collected by a Omnistar quadrupole mass spectrometer (Pfeiffer), and data analysis (deconvolution) was carried out using OriginPro software package.

### 2.2.5 Pyridine FT-IR spectroscopy

Self-supporting wafers of the TiO<sub>2</sub> materials were first pre-treated at 400 °C and 1 mbar vacuum for 1 h. To evaluate the potential presence of Lewis (L) and Brønsted (B) acid sites, the TiO<sub>2</sub> wafers were then saturated with pyridine probe at 50 °C (25 mbar pyridine vapor). Prior to data collection at 150 °C, the samples were degassed at 150, 250 or 350 °C. Using 256 scans per spectrum and 2 cm<sup>-1</sup> resolution, analysis was carried out on a Nicolet 6700 spectrometer with DTGS detector. A Lewis acid extinction coefficients ( $\epsilon(L)$ ) value of 1.63 cm/μmol was used.[36, 37]

### 2.2.6 UV-vis diffuse reflectance spectroscopy

The TiO<sub>2</sub> samples were pelletized between 250–500 μm and put into a quartz U-tube with UV–vis transparent window. Pre-treatment was carried out in N<sub>2</sub> flow at 300°C (5 °C/min heating rate) for 1 h. Afterwards, data recording was performed at room temperature in nitrogen atmosphere for wavenumber values ranging from 4000 to 50000 cm<sup>-1</sup>. All spectra were corrected for background signals using dried BaSO<sub>4</sub> pellets as reference. A Cary 5000 UV–vis–NIR spectrophotometer (Agilent) was used for all measurements. The final results are displayed by the Kubelka–Munk function.

## 2.3 Ketonization reaction

### 2.3.1 Reaction procedure

For the ketonization reactions, the fatty acid substrate, n-dodecane solvent and TiO<sub>2</sub> catalyst (wt% loading expressed as  $m_{\text{catalyst}}/m_{\text{substrate}}$ ) were added into a 100 ml Parr reactor. Inertization of the reaction atmosphere was ensured by repeating the same N<sub>2</sub> flushing procedure (10 bar N<sub>2</sub>, stirring at 600 rpm for 1.5 min, evacuating headspace) three times. The desired ketonization temperature was then reached by heating from room temperature. With the experimental set-up, the reactor is entirely surrounded by the heating mantle which fully encompasses the reactor, including the head space. Semi-batch ketonization experiments at constant pressure were defined by addition of a continuous N<sub>2</sub> flow through the liquid phase during reaction. The input of this flow was controlled by BRIGHT modules (Bronkhorst), with back pressure regulators maintaining a constant reactor pressure. The gasses at the reactor outlet were passed through a condenser set at 5°C, without losing any fatty acids or ketones. After ketonization, the system was cooled to 50 °C and depressurized before further analysis.

### 2.3.2 Product analysis

For product analysis, 0.5 g of internal standard (eicosane) was added and the reaction medium was stirred for 10 min. Then 3 mL chloroform was added to 1 mL sample. To remove any remaining TiO<sub>2</sub> from this mixture,

centrifugation was carried out for 15 min at 3500 rpm. The supernatant was derivatised with MSTFA (5 times molar excess) at 60 °C for 1 h to silylate any remaining fatty acid molecules. Using N<sub>2</sub> carrier gas, a 6890 gas chromatography instrument (Agilent) with HP-5 column (30 m, 0.32 mm internal diameter, 0.25 µm film thickness) and flame ionization detector (320 °C) was used to analyse the composition of the reaction mixture (1 µl injection volume, 10:1 split ratio, 300 °C injection temperature). Starting from 60 °C, the oven temperature was increased to 190 °C (10 °C/min heating rate), from 190 °C to 200 °C (1 °C/min ramp) and from 200 °C to 310 °C at 5 °C/min. The final temperature was held for 15 min. Standard calibration curves, obtained with the analytical grade fatty acids and ketones, were used to quantify these results. A 5973 gas chromatography-mass spectrometry instrument (Agilent) with HP-5ms column (25 m, 0.25 mm internal diameter, 0.25 µm film thickness) was used to identify any unknown compounds.

### 2.3.3 Kinetic analysis

For the kinetic experiments, the reaction time was set to  $t=0$  once the target temperature was reached. Any conversion of substrate to products that occurred during the heating window was accounted for by appropriately adjusting the  $C_0$  compound concentrations at  $t_0$ . For all kinetic experiments, the total substrate conversion values were kept below 53%. Carbon mass balances were >97% for all experiments. Parameter estimation by linear regression analysis of reaction data was done by OriginPro software. For the Langmuir-Hinshelwood kinetic models, multiple non-linear regression was performed with XLSTAT software by Addinsoft[38] using a numerical iterative Levenberg-Marquardt algorithm to minimize the objective function (sum of square of errors). A confidence level of 95% was used throughout this study for statistical analysis.

## 3. Results and discussion

### 3.1 Catalyst characterization

The two commercial TiO<sub>2</sub> catalysts were characterized prior to screening their ketonization activity. The crystal phases of both materials were verified via PXRD, indicating pure anatase (A) and rutile (R) phases (Figure 1A). For A TiO<sub>2</sub>, the dominant crystal surface was (101), situated at a  $2\theta$  value of 26 degrees. For R TiO<sub>2</sub>, the (110) surface was most abundant (with a  $2\theta$  value of 28 degrees).[39] Using the Scherrer equation, apparent primary crystallite (domain) sizes of 7.8 and 11.6 nm were obtained for A and R, respectively. These values are in line with the primary crystallite size as, provided by the manufacturers. The DRS UV-vis measurements also accord to the presence of these crystal structures as band gap energies of 3.3 and 3.05 eV were found (Kubelka-Munk theory) for anatase and rutile TiO<sub>2</sub>, respectively (Supporting information, Figure S1A). This is in good agreement with typical reported values for these different crystal phases.[40] Scanning electron microscopy images show for both materials that the primary (nanosized) crystals aggregate into larger heterogeneously (micrometer) sized particles (Figures 1B and 1C). The BET surface area, total pore volume and pore diameter parameters were determined via N<sub>2</sub> physisorption with 266 m<sup>2</sup>/g, 0.36 cm<sup>3</sup>/g and 5.1 nm for A, and 77 m<sup>2</sup>/g, 0.63 cm<sup>3</sup>/g and 38 nm for R TiO<sub>2</sub>, respectively.

The acid-base properties were determined by temperature programmed desorption (TPD) of NH<sub>3</sub> and CO<sub>2</sub> probes, and by FT-IR spectroscopy with pyridine as probe molecule. The broad signals of the TPD measurements were deconvoluted to distinguish acid-base sites with different strength (Supporting information, Figures S1B-S1E). For

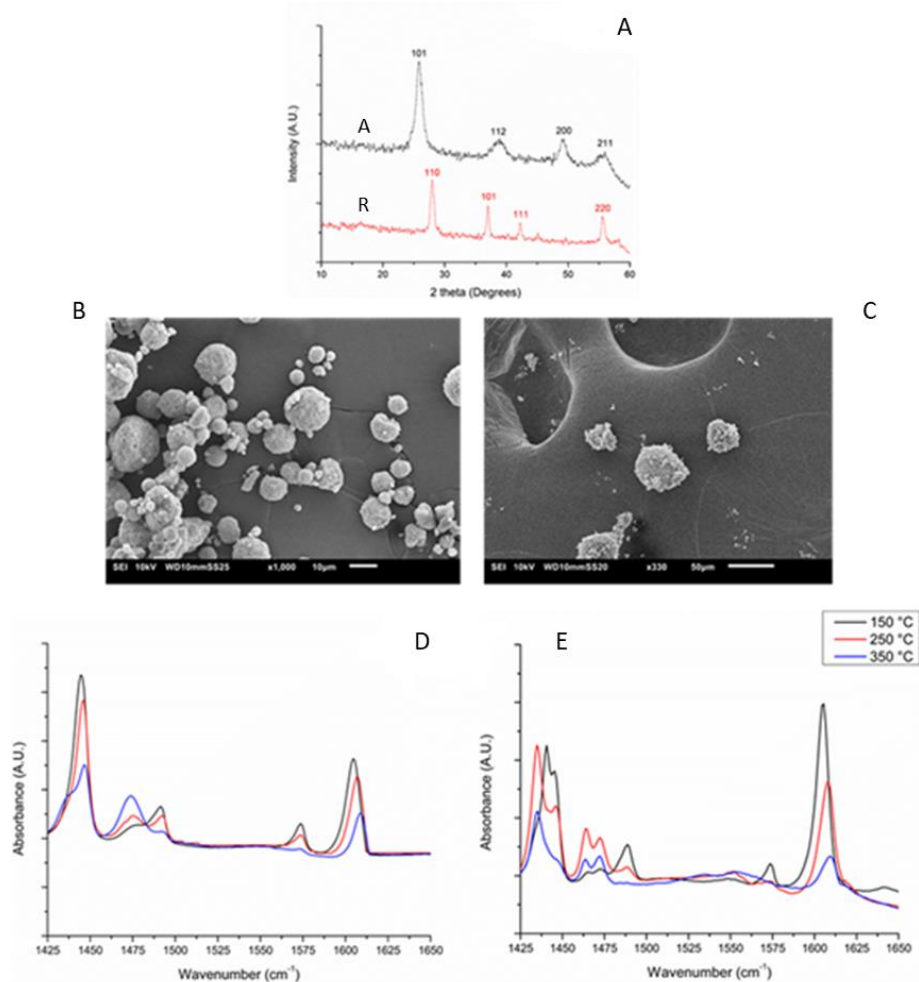


Figure 1: PXRD of anatase (A) and rutile (R) (A); SEM of R (B) and A (C); Pyridine IR measurements at 150, 250 and 350 °C for A TiO<sub>2</sub> (D) and R TiO<sub>2</sub> (E).

NH<sub>3</sub> TPD analysis of anatase TiO<sub>2</sub>, desorption maxima were found at 238, 317 and 427 °C, which were assigned to weak (16%), medium (53%) and strong (31%) acid sites, respectively. For rutile TiO<sub>2</sub>, these maxima occurred at higher desorption temperatures of 270 °C (32%), 401 °C (58%) and 611 °C (10%). The desorption of NH<sub>3</sub> base at lower temperatures for A indicates weaker bonding of the probe molecule with the Lewis acid surface sites, and thus lower acid site strength compared to the active sites of R. Next, CO<sub>2</sub> was used as acid probe molecule to determine the basicity of both catalysts. The use of this probe is particularly interesting for the ketonization reaction, as CO<sub>2</sub> is also one of the reaction products. For A TiO<sub>2</sub>, two broad desorption signals between 50-225 °C (70%) and 425-800 °C (30%) were observed, indicating the presence of weaker and stronger Lewis base sites, respectively. The R catalyst mainly showed a broad signal between 50-300 °C (90%), and two smaller signals between 450-600 °C (5%) and 625-800 °C (5%), indicating that A TiO<sub>2</sub> has a higher percentage of basic sites which interact more strongly with the CO<sub>2</sub> probe. Integration of the CO<sub>2</sub> signal revealed that the total basicity is higher for A TiO<sub>2</sub>, when expressed in terms of both catalyst surface area and weight.

Table 1: Summary of characterization results of anatase (A) and rutile (R) TiO<sub>2</sub> catalysts used in this work.

Catalyst property	Anatase (A)	Rutile (R)	R/A ratio
Primary crystallite size (nm)*	7.8	12.8	NA
Band gap (eV)	3.3	3.05	0.92
BET surface area (m <sup>2</sup> /g)	266	77	0.29
Pore volume (cm <sup>3</sup> /g)	0.36	0.63	NA
Pore diameter (nm)	5.1	38	NA
Lewis acidity (μmol/g) at 150°C	324	133	0.41
Lewis acidity (μmol/m <sup>2</sup> ) at 150°C	1.22	1.73	1.42
Lewis acidity (μmol/m <sup>2</sup> ) at 250°C	0.86	1.61	1.87
Lewis acidity (μmol/m <sup>2</sup> ) at 350°C	0.42	0.72	1.71
Bronsted acidity (μmol/g) at 150°C	<1	<1	NA
Relative acidity** (%)	100	273	2.73
Relative basicity** (%)	100	62	0.62

\* Based on XRD

\*\* Based on total integrated TPD signal area per surface area of catalyst

NA: Not applicable

Pyridine probe FT-IR spectroscopy was performed to discriminate between Lewis and Brønsted acid sites. Rutile TiO<sub>2</sub> showed characteristic Lewis acid site absorption bands at 1441, 1489, 1575 and 1605 cm<sup>-1</sup> (Figure 1E). Given no signals at 1545 and 1635 cm<sup>-1</sup>, absence of Brønsted acid sites can be assumed. The quantity and strength of the coordinatively unsaturated Ti<sup>x+</sup> surface species was investigated by determining the amount of chemisorbed pyridine probe at different temperatures. Quantification of the FT-IR analysis resulted in acid site density values of 1.73, 1.61 and 0.72 μmol/m<sup>2</sup> at 150, 250 and 350 °C, respectively. At the highest temperature, 42% of the chemisorbed pyridine remained on the catalyst surface, indicating presence of strong Lewis acid sites. Similarly, A TiO<sub>2</sub> is characterized by Lewis acid absorption bands at 1445, 1492, 1575 and 1606 cm<sup>-1</sup>, with no significant amounts of Brønsted acid sites (Figure 1D). For this catalyst, the acid site density values at 150, 250 and 350 °C were 1.22, 0.86 and 0.42 μmol/m<sup>2</sup>, respectively. Compared to rutile, this indicates weaker interaction between the chemisorbed pyridine probe and the Lewis acid surface sites on anatase, as more pyridine desorbed at the higher temperatures. Overall, R has a higher acid site density on a surface area basis, while A has a higher amount of acid sites per catalyst weight. In summary, both commercial catalysts are pure phase amphoteric TiO<sub>2</sub> materials with distinct (Lewis) acid-base properties (Table 1).

### 3.2 Fatty acid ketonization and mass transfer

An initial study of the ketonization activity of both TiO<sub>2</sub> catalysts was performed in the liquid phase using lauric acid (C12:0) as a model fatty acid compound (Figure 2). Since H<sub>2</sub>O and CO<sub>2</sub> are formed during reaction, the mass yield of C<sub>23</sub> laurone is limited to a maximum value of 84.5% at full lauric acid conversion. Dodecane was used as inert reaction solvent, allowing variations in initial substrate and product concentrations.



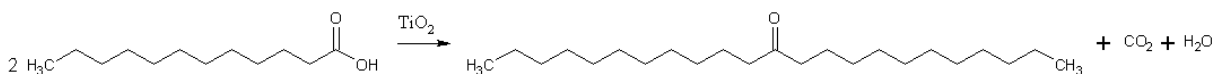


Figure 2: Ketonization of lauric acid to laurone, CO<sub>2</sub> and H<sub>2</sub>O with a TiO<sub>2</sub> catalyst.

Figure 3A displays the evolution of lauric acid (LA) concentration over time during ketonization with 10 wt% TiO<sub>2</sub> catalysts (powder form) in a closed batch reactor operating at 340 °C and autogenous pressure (9.5 bar) with a stirring rate of 600 rpm. The results clearly show that R has a higher (initial) ketonization activity for a similar catalyst weight. Under these conditions, the ketonization selectivity was always  $\geq 98\%$  for both catalysts.

Before conducting further kinetic experiments, it is important to exclude that any diffusion issues are determining this observed activity. To determine whether these results represent intrinsic activity in the chemical regime, the potential presence of mass transfer limitations was studied. External mass transfer limitations were investigated by varying the stirring rate between 75-800 rpm (Figure 3B). It can be seen that increasing the stirring rate from 75 to 300 rpm resulted in a minor conversion rate increase for both catalysts, viz. 12% for A and 4% for R, respectively. A further increase from 300 rpm to 600-800 rpm again (slightly) increased the reaction rates by 3%. There was no difference in the 600-800 rpm range and therefore 600 rpm was chosen as a suitable stirring rate in this study to guarantee exclusion of external mass transfer limitations, which will also be evidenced further when determining the activation energy values. Next, internal mass transfer limitations were investigated using the Weisz-Prater Criterion ( $C_{WP}$ ), assuming spherical and isothermal particles (Supporting Information). The intrinsic observed reaction rates were taken from the initial C(t) part, equalling  $9.0 \cdot 10^{-4}$  and  $50 \cdot 10^{-4}$  M/m<sup>2</sup>h for A and R TiO<sub>2</sub>, respectively (or 2.5 and 4.0 g/g<sub>cat</sub>h in terms of weight). The true catalyst densities are 3.9 and 4.2 g/cm<sup>3</sup> for A and R, respectively, as provided by the manufacturer via pycnometer measurement. Based on analysis of the SEM images (Supporting Information, Figure S2), a particle radius value of 30  $\mu\text{m}$  was chosen as a reasonable upper limit to avoid any underestimation of  $C_{WP}$  for both catalysts. The bulk diffusivity of the substrate was calculated by the Wilke-Chang equation and verified with reported values of similar reaction systems (Supporting Information).[41, 42] For

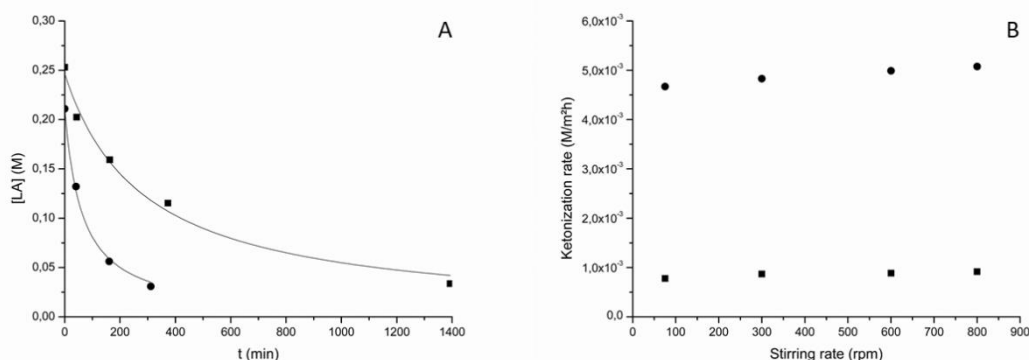


Figure 3: C(t) plot for ketonization of lauric acid with A (■) and R (●) TiO<sub>2</sub>, with full lines representing second order reaction fitting. Reaction conditions: 15 mmol LA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C – 600 rpm – autogenous pressure (A); Ketonization rate of lauric acid in function of stirring rate. Reaction conditions: 15 mmol LA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C – 45 min – autogenous pressure (B).

an initial substrate loading of 15 mmol, the concentration of lauric acid at the catalyst surface is set equal to the bulk concentration since external mass limitations were excluded earlier. As a final result, the calculated effective diffusivity values are  $7.26 \cdot 10^{-9}$  and  $7.34 \cdot 10^{-9}$  m<sup>2</sup>/s for A and R, respectively, which ultimately results in  $C_{WP}$  values of  $6.6 \cdot 10^{-3}$  and  $1.4 \cdot 10^{-2}$  (Supporting Information). Since both values are  $\ll 1$ , it can be stated that no internal mass transfer limitations are present under the applied reaction conditions, which implies that the experimental data presented under these conditions are governed by the catalytic reactions occurring in the chemical regime.

Based on the C(t) profiles of Figure 3A, it was found that a second order reaction model best described the experimental data (Supporting Information, Figure S3 and Table S1). Physically, the ketonization reaction may adhere to a second order model since the bimolecular coupling requires two adsorbed carboxylic acids at the catalyst surface. It must be noted that the experimental data do not exclude the possibility of a first order model ( $p < 0.05$ ). From a physical standpoint, this may apply for ketonization when acid molecules are readily adsorbed on the catalyst surface, awaiting the adsorption of a second molecule on an adjacent active site for the C-C coupling. In this case, the ketonization rate may be linearly proportional to the substrate concentration. The latter may be more probable at higher substrate concentrations. The slopes of the second order models in Figure S3 were used to determine the second order rate constants of A ( $0.014 \pm 0.002 \text{ M}^{-1} \text{ min}^{-1}$ ) and R ( $0.076 \pm 0.005 \text{ M}^{-1} \text{ min}^{-1}$ ). Finally, the Thiele modulus ( $\varphi_{pn}$ ) and reaction efficiency ( $\eta$ ) values were calculated (Supporting Information). Based on the experimental data, the Thiele modulus values are  $1.1 \cdot 10^{-3}$  and  $2.3 \cdot 10^{-3}$  for A and R TiO<sub>2</sub>, respectively. These correspond with 99.9% reaction efficiency for both catalysts, confirming again that the reaction rate is indeed determined by the catalytic reaction, and the data are not interfered by mass transfer limitation phenomena.

### 3.3 Kinetics of fatty acid ketonization in liquid phase

#### 3.3.1 Impact of substrate and catalyst loading

Both the initial substrate concentration and catalyst loading were varied to determine their impact on the ketonization activity. First, the initial lauric acid loading was varied between 0-30 mmol (Figure 4). The general R(C<sub>0</sub>) trend is rather similar for both TiO<sub>2</sub> catalysts, alluding to the existence of two regimes. At lower lauric acid concentrations, there is a larger impact of substrate concentration on the ketonization rate, while the reaction rate curves start to flatten for higher concentrations. From these data, the observed reaction orders  $n$  were determined in the applied concentration ranges for both catalysts by linearization of the power law (eq. 1):

$$R_{obs} = k_{obs}[LA]^n \quad (1)$$

with  $R_{obs}$  the observed reaction rate (in M/m<sup>2</sup>h),  $k_{obs}$  the observed rate constant,  $[LA]$  the lauric acid concentration and  $n$  the observed reaction order. For A TiO<sub>2</sub>, the overall observed reaction order is  $0.39 \pm 0.02$  (Figure S4A). For the R catalyst, the  $n$  value is significantly higher at  $0.55 \pm 0.07$  (Figure S4B). These observed fractional orders indicate a lauric acid concentration range for the bimolecular ketonization reaction in which a state of saturation of catalytic active sites is approached for high fatty acid concentrations, where the ketonization rate will no longer increase for higher initial lauric acid loadings. As stated in the introduction, this has also been observed by others for C<sub>2</sub>-C<sub>4</sub> gas-phase ketonization reactions. Furthermore, the observed orders differ significantly between both catalysts, suggesting a difference in substrate-surface interaction. An initial substrate loading of 15 mmol lauric acid was

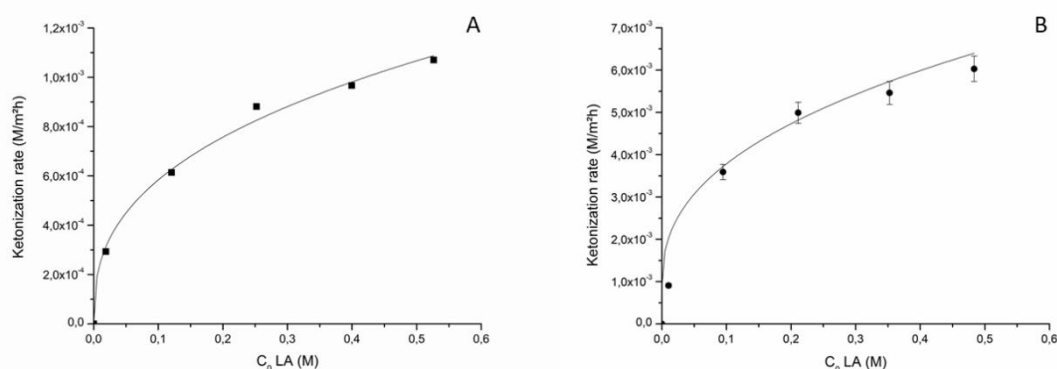


Figure 4: Ketonization rate in function of initial lauric acid concentration for A (A) and R (B) catalysts. The full lines represent fitting of the power law equation  $R_{obs} = k_{obs}[LA]^n$  with  $n = 0.39$  for A, and  $n = 0.55$  for R. Reaction conditions: 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C – 45 min – 600 rpm – autogenous pressure.

chosen for further investigation as it grants sufficient possibilities to vary catalyst and product loadings in the next paragraphs, while taking into account compound solubilities and allowing the ketonization rates to vary up to at least an order of magnitude.

The influence of the catalyst loading was investigated in the range of 2.5-20 wt% at a constant initial lauric acid concentration (Figure S5). For both catalysts, the ketonization rate (expressed on surface area basis) was reduced for a higher loading of 20 wt%. This reduction was more severe in the case of the R catalyst (39%) compared to the A material (14% reduction). For both catalysts it may indicate an upper limit of substrate adsorption, flocculation/aggregation of catalyst particles with loss of added surface area, higher viscosity of the reaction medium, and related to that limited mass transfer or other phenomena which reduce the activity per added surface area for higher catalyst loadings. The R TiO<sub>2</sub> catalyst may be more prone to the flocculation/aggregation effects. Furthermore, its higher intrinsic turnover rate is also accompanied by a higher sensitivity to product inhibition (section 3.3.3), which may become more pertinent at the highest catalyst loading of 20 wt% due to fast initial product formation. The catalyst loading of 10 wt% was therefore selected for further kinetic study.

As a reference, thermal ketonization experiments were also carried out in absence of any TiO<sub>2</sub> catalyst (Supporting Information, Figure S6). After a total time of 90 minutes (including heating phase), the total lauric acid conversion only reached 4.4% with 69% selectivity to the laurone product, equalling a 10 mM/h initial conversion rate and 3.6 mM/h ketone productivity. In comparison, the experiments carried out with A TiO<sub>2</sub> always showed >98 % ketone selectivity, with initial conversion rate values of 22-113 mM/h for 2.5-20 wt% catalyst loading, equalling 11-57 mM/h ketone productivity rates. In other words, the ketone productivity increased by a factor of 3.1-16 compared to the thermal ketonization experiment without formation of unwanted side products. For the R TiO<sub>2</sub> catalyst, these lauric acid conversion and ketone productivity values are even higher, with 4.1-17 times higher ketone productivity for 2.5-20 wt% catalyst loading. For a longer total time of 270 min in absence of catalyst, the lauric acid conversion was 16.1% with 61% selectivity for laurone. These values are significantly lower than those obtained in the presence of either A or R catalyst. For example, already after 210 min the total lauric acid conversion values were 43% and 80% for 10 wt% loading of A and R, respectively, with full selectivity to the desired ketone product. Our data

unambiguously show that the presence of the heterogenous catalyst is preferred to achieve fast ketonization reactions with high product yields and selectivity.

### 3.3.2 Temperature dependency of liquid phase catalytic ketonization

The influence of the reaction temperature was studied between 300-340°C to determine the (apparent) activation energy, observed enthalpy, entropy and Gibbs free energy of activation. As shown in Figure S7, increasing the reaction temperature from 300 to 340 °C significantly increased the ketonization rate for both catalysts, revealing an exponential relationship in agreement with Arrhenius law. From these results, apparent activation energies of  $137 \pm 7$  kJ and  $117 \pm 5$  kJ/mol were determined for A and R, respectively. These values for liquid phase catalysis are in good agreement with other reported values for gas-phase ketonization, viz. 105 and 116 kJ/mol for 2-methylbutanoic acid and pentanoic acid on  $ZrO_2$ [43], 132 kJ/mol for acetic acid on KOH treated  $ZrO_2$ [44], 92-124 kJ/mol on isolated  $ZrOH$ [45] and 124 kJ/mol for propanoic acid on Zn-Cr mixed oxide.[46] Higher values have also been published, such as 185 kJ/mol for  $C_2$  acid ketonization with  $Ru/TiO_2$ [17], 160 kJ/mol for C-C coupling of pure  $C_{16}$  acid on  $K_2O/TiO_2$ [47] and 177 kJ/mol for palm fatty acid distillate ketonization on  $TiO_2$  in liquid phase.[6] The substrate and catalyst, but also the reactor system and operational conditions clearly impact the observed activation energy values. Our results conclude that under the applied reaction conditions in a batch reactor, the activation energy values differ significantly between both  $TiO_2$  phases and that ketonization of fatty acids is kinetically more favourable on the rutile phase, compared to anatase  $TiO_2$ .

The temperature dependent conversion data were used to get more insight into the thermodynamics of the transition state. In Figure 5, the Eyring-Polanyi equation of transition state theory was plotted to identify the contribution of the activation enthalpy and entropy to the Gibbs free energy of activation for lauric acid ketonization. The slopes of both curves were used to calculate  $\Delta H^\ddagger$ , while  $\Delta S^\ddagger$  can be derived from the intercepts (Supporting Information). For A  $TiO_2$ , the  $\Delta H^\ddagger$ ,  $\Delta S^\ddagger$  and  $\Delta G^\ddagger$  parameters for the rate determining step (C-C coupling, see kinetic model paragraph) are  $137 \pm 7$  kJ/mol,  $-121 \pm 19$  J/mol.K and  $204 \pm 16$  kJ/mol, respectively, at 340 °C (Table 2). For R, these values are  $112 \pm 5$  kJ/mol,  $-147 \pm 22$  J/mol.K and  $203 \pm 15$  kJ/mol, respectively, for the rate determining

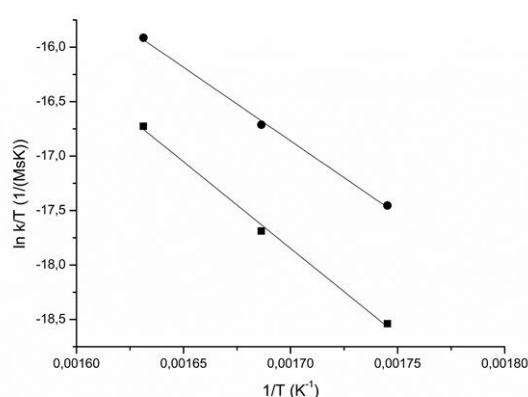


Figure 5: Eyring-Polanyi plot to determine  $\Delta H^\ddagger$ ,  $\Delta S^\ddagger$  and  $\Delta G^\ddagger$  for lauric acid coupling on A (■) (adj.  $R^2=0.99$ , F-value = 335, p-value= 0.03) and R (●) (adj.  $R^2=0.99$ , F-value = 613, p-value= 0.03)  $TiO_2$ .

step. These data indicate that for A and R TiO<sub>2</sub>, the enthalpy term has a larger contribution to the Gibbs free energy of activation than the entropy for the studied ketonization temperature range. Furthermore, the enthalpy terms differ significantly between both catalysts, which is not the case for the activation entropy. The formation of the transition state (TS) is characterized by a loss of entropy, which agrees with the associative nature of the bimolecular C-C coupling of carboxylic acids to produce an activated complex. Some  $\Delta S^\ddagger$  values have been reported for gas-phase ketonization before, such as -90 and -135 J/mol.K for pentanoic and 2-methylbutanoic acid on ZrO<sub>2</sub>, for example.[43] Oppositely, positive  $\Delta S^\ddagger$  values have also been stated for C<sub>2</sub>-C<sub>4</sub> acid ketonization[25], although this possibility of a TS with more degrees of freedom is counterintuitive. A combination of kinetic experiments and DFT calculations using anatase TiO<sub>2</sub> for acetic, propanoic and butyric acid coupling revealed  $\Delta G^\ddagger$  values ranging between 166 and 176 kJ/mol at 250°. For the reaction of acetic acid,  $\Delta H^\ddagger$  was 137 kJ/mol with  $\Delta S^\ddagger$  equal to -56 J/mol.K at 230 °C.[13] When using ZrO<sub>2</sub>,  $\Delta G^\ddagger$  values varied between 157 and 168 kJ/mol for the different acid substrates.[14] Our data for the liquid phase ketonization of fatty acids is largely in accordance with the reports for gas-phase ketonization of shorter acids.

Table 2: Summary of Arrhenius and Eyring-Polanyi analysis for lauric acid ketonization on A and R TiO<sub>2</sub> at 340°C.

	Anatase (A)		Rutile (R)		P-value*
	Value	95% CI	Value	95% CI	
<b>E<sub>a,obs</sub> (kJ/mol)</b>	137 ± 7	129,145	117 ± 5	111,123	0.02
<b>ΔH<sup>‡</sup> (kJ/mol)</b>	132 ± 7	124,140	112 ± 5	106,118	0.02
<b>ΔS<sup>‡</sup> (J/mol.K)</b>	-121 ± 19	-99,-143	-147 ± 22	-122,-172	0.19
<b>ΔG<sup>‡</sup> (kJ/mol)</b>	206 ± 16	188,224	203 ± 15	186,220	0.82

\*2 sample t-test

### 3.3.3 Product inhibitory effects

Prior to the construction of a kinetic model for both catalysts, the possibility of product inhibition was examined in more detail. This includes all three ketonization products, namely ketone, H<sub>2</sub>O and CO<sub>2</sub>. First, the potential effect of the ketone product was assessed experimentally by adding pure C<sub>27</sub> myristone (14-heptacosanone, CH<sub>3</sub>(CH<sub>2</sub>)<sub>12</sub>C=O(CH<sub>2</sub>)<sub>12</sub>CH<sub>3</sub>), the ketonization product of myristic acid (C<sub>14:0</sub>), at the start of reaction. Up to 8.2 mmol ketone was added, covering the entire conversion range of lauric acid since the maximum theoretical yield of laurone is 7.5 mmol when 15 mmol lauric acid substrate is used. Myristone is used as an analogue model for laurone to reduce analytical complexity, assuming that its potential impact is comparable to that of laurone due to their very high degree of similarity. Furthermore, it is assumed that the ketone is entirely present in the liquid phase under reaction conditions, given its 440-450 °C boiling point. As can be derived from Figures 6A and 6B, there is indeed a significant negative impact of the ketone product on the ketonization rate, albeit to a different degree for both TiO<sub>2</sub> catalysts. For A, the ketonization rate drops gradually for increasing ketone concentrations, showing a 15% decrease in activity in presence of 0.08 M myristone. Any additional concentration increase of ketone did not further lower the ketonization rate. Using a power law equation, a minor but significant negative experimental reaction order of -0.07 ± 0.01 was calculated for the ketone product in this entire concentration range (Figure S8A). In contrast, a much larger negative impact was found for R TiO<sub>2</sub>, for which a low initial myristone concentration already resulted

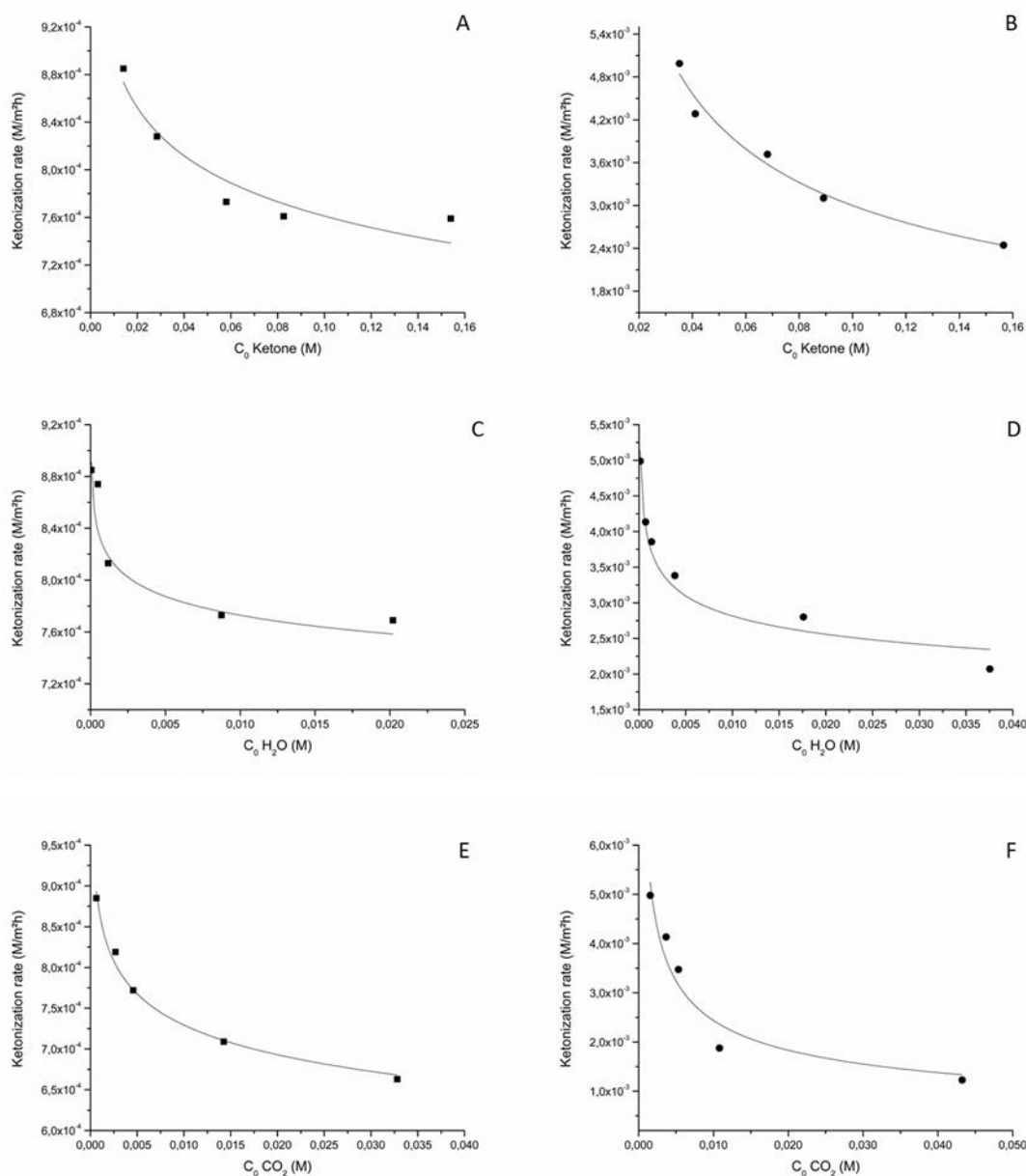


Figure 6: Ketonization rate in function of initial myristone concentration for A (A) and R (B) TiO<sub>2</sub>. Ketonization rate in function of initial effective water concentration for A (C) and R (D) TiO<sub>2</sub>. Ketonization rate in function of initial effective CO<sub>2</sub> concentration for A (E) and R (F) TiO<sub>2</sub>. The full lines represent fitting of the power law equations with the experimentally derived observed product reaction orders. Reaction conditions: 15 mmol LA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C - 45 min - 600 rpm – autogenous pressure.

in a significantly steep decline of the acid conversion rate. Furthermore, the negative trend is continued for higher concentrations, albeit to a lesser extent than the initial activity drop. For instance, an initial myristone concentration of 0.15 M led to a more than halving of the reaction rate. From these results, a negative order of  $-0.46 \pm 0.03$  was determined for the R catalyst, indicating a significantly higher sensitivity to ketone inhibition compared to A (Supporting Information, Figure S8B). These observations suggest competitive adsorption of the ketone product on

the active sites via its carbonyl group, reducing their availability for carboxylic acid substrate molecules and the ketonization reaction.

Besides ketone, also the impact of H<sub>2</sub>O on the conversion rate was studied. Here liquid distilled water, in the range of up to 167 mmol, was added at the start of reaction. Note that 15 mmol is the maximum theoretical yield of H<sub>2</sub>O at full lauric acid conversion. Compared to the ketone product, the kinetic effect is more complex to describe as the majority of the added water will appear in the head space as vapour during reaction due to the high ketonization temperature. The interaction between water and the reaction solvent should also be considered in this case as water is poorly soluble in dodecane. Therefore, the effective initial water concentration in the liquid phase was estimated based on calculations that combine the observed total system pressure and extrapolation of literature data regarding the solubility of water in dodecane at elevated temperatures.[48] Depending on the initial loading, the molar fraction of water in the liquid dodecane phase is only between 0.36-1.2% at 340 °C. As a result, the effective initial water concentration at reaction temperature varies approximately up to 37 mM (while adding a maximum of 3.1 M, not taking into account vapour pressure and solubility factors). Figures 6C and 6D present the effect of water on the ketonization rate for both catalysts in terms of the initial calculated effective concentrations. The experiments show a significant negative impact on the ketonization rate for both materials, although the trend and strength of the inhibitory effect is different. The A catalyst undergoes a drop in conversion rate in the presence of water, but the reaction rate stabilizes at 87% of the initial activity for effective water concentrations of 9 mM and higher as an increase to 20 mM did not have a further negative impact (Figure 6D). Analysis of these experiments reveals a minor (but significant)  $-0.03 \pm 0.005$  observed reaction order for water (Figure S8C). The water inhibitory effect was also observed for R, although for this catalyst there is a continuous decline of the ketonization rate for the whole concentration range tested (Figure 6E). In contrast to A TiO<sub>2</sub>, the ketonization rate still decreases above effective water concentrations of 9 mM. For instance, the reaction rate is reduced by 44% at 18 mM and by 59% at 37 mM (highest initial water concentration). The overall observed reaction order of water for this entire concentration range is  $-0.16 \pm 0.02$  for the R catalyst (Supporting information, Figure S8D). This difference in trend and strength of water inhibition show a more pronounced sensitivity for the more active R material. For both catalysts, the origin of the water inhibition effect is more complex than that of the ketone product, since more factors could contribute to its negative impact on the catalytic activity. Firstly, competitive adsorption of water on the active surface sites is possible via the water hydroxyl groups. Secondly, the H<sub>2</sub>O molecules (formed during ketonization) could also partake in forward and reverse (de)protonation elementary reaction steps.[33] Thirdly, the catalyst surface may also become the subject of hydrothermal breakdown (e.g. TiO<sub>2</sub> phase transitions or sintering with reduction of surface area) under the ketonization conditions, which can impact its catalytic performance (see Supporting Information for post-reaction SEM analysis, Figure S9). The R catalyst remains the most active TiO<sub>2</sub> material, even though it is more susceptible to the inhibitory effect of the H<sub>2</sub>O ketonization by-product.

Thirdly, the effect of CO<sub>2</sub> was determined experimentally by initially pressurizing the batch reactor with external CO<sub>2</sub> (up to 12 bar) at room temperature before heating. The results are shown in Figures 6E and 6F, and it must be noted first that reference experiments under inert N<sub>2</sub> atmosphere at various pressures were performed to rule out any overall pressure effect. We found no effect of the total system pressure on the rate of reaction for the studied pressure range. As such, the observations in Figure 6 are directly related to the presence of CO<sub>2</sub>. As was the case for water, the initial CO<sub>2</sub> concentration in the liquid phase was estimated to be able to calculate its effective kinetic

inhibitory effect on the ketonization catalysis (since the largest part will be in the head space). This estimation uses extrapolation of available literature data regarding the solubility of CO<sub>2</sub> in liquid hydrocarbons at elevated temperatures and pressures.[49] The molar fraction of CO<sub>2</sub> in dodecane at 340 °C is around 4.4-9.1%, depending on the total system pressure, and was used to determine the effective initial CO<sub>2</sub> concentrations in the liquid phase, which maximizes at 43 mM (for initial pressures up to 12 bar). Note that 140 mM is the maximum theoretical concentration of CO<sub>2</sub> at full lauric acid conversion if 100% of the formed CO<sub>2</sub> is solubilized in the liquid phase reaction medium. For A TiO<sub>2</sub>, the ketonization rate declines continuously, with a 25% reduction of the reaction rate at 32 mM CO<sub>2</sub>. A similar but more severe trend can be observed for R TiO<sub>2</sub>, as its ketonization activity is reduced by 75% for 43 mM CO<sub>2</sub>. Analysis of these experimental data reveals negative observed reaction orders of  $-0.07 \pm 0.004$  and  $-0.46 \pm 0.06$  for the A and R catalysts, respectively (Figures S8D and S8E). The negative impact of carbon dioxide may be attributed to competitive adsorption on the surface sites. Although the environments surrounding the catalysts are different than during liquid phase reaction in dodecane, the CO<sub>2</sub> TPD experiments have shown that CO<sub>2</sub> desorption still occurs above the reaction temperature of 340 °C for both catalysts. Surface carbonates may be formed, or bicarbonates in co-presence of water, deactivating the TiO<sub>2</sub> surfaces for further ketonization.[50, 51] Since there are no reports on these inhibitory effects for liquid phase ketonization, direct comparison with literature data cannot be made. However, there is mentioning of a recent patent application on continuous liquid phase fatty acid ketonization with TiO<sub>2</sub> that employs the CO<sub>2</sub> by-product as carrier gas[47], which seems inadvisable based on our data. In the referenced work, water is stripped from the condensed phase by the recycled CO<sub>2</sub> to counteract active site inhibition by H<sub>2</sub>O. Here, only the latter has been taken into account, while our study shows that the inhibition of CO<sub>2</sub> could at least be as important, if not more. These experiments unambiguously show that inhibition from all products should be considered when performing fatty acid ketonization reactions in the liquid phase. Furthermore, the more active R catalyst is most prone to such inhibition (compared to A TiO<sub>2</sub>) for all reaction products, which is demonstrated experimentally for the first time in this work for liquid phase fatty acid ketonization (Table S2). In conclusion to this part and by using the experimentally derived reaction orders, the observed ketonization rates can be expressed as power laws according to equations 2 and 3 for A and R TiO<sub>2</sub>, respectively.

$$R_{A,obs} = k_{A,obs} [C_{Acid}]^{0.39} [C_{ketone}]^{-0.07} [C_{H2O}]^{-0.03} [C_{CO2}]^{-0.07} \quad (2)$$

$$R_{R,obs} = k_{R,obs} [C_{Acid}]^{0.55} [C_{ketone}]^{-0.46} [C_{H2O}]^{-0.16} [C_{CO2}]^{-0.46} \quad (3)$$

### 3.3.4 Irreversibility of liquid phase ketonization and the re-ketonization side reaction

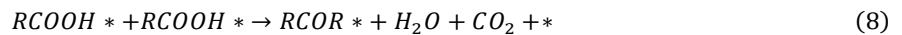
In a recent gas phase study, it has been shown that under specific conditions, the reaction products could undergo the reverse ketonization reaction to the original acid substrates.[52] Additionally, a diketone intermediate may be formed as a result of the re-ketonization side reaction between a carboxylic acid and ketone molecule.[53] This condensation intermediate can either decompose back to the original acids in case of homo-ketonization, or create new ketones during cross-ketonization. Therefore, it is important to consider and investigate the possibilities of equilibrium and re-ketonization for liquid phase fatty acid ketonization. Experiments arguing such equilibrium were



described earlier in this contribution, and studied the impact of the inhibitory effect of the ketone product. When adding C<sub>27</sub> myristone to the reaction mixture, significant equilibrium would have led to the formation of the C<sub>25</sub> ketone cross-product. However, no such ketone was detected, indicating that at least in our conditions, re-ketonization does not occur. Furthermore, myristic acid was also not observed in these experiments. To further corroborate the irreversibility of ketonization, an additional experiment was carried out in the presence of C<sub>35</sub> stearone (18-pentatriacontanone). The reaction was monitored for longer reaction times, viz. 4.5 hours, and higher concentration of stearone was added (lauric acid and stearone were added in a 1:1 weight ratio). Although these modified conditions are more favourable to enable cross-coupling, no C<sub>29</sub> ketone (12-nonacosanone) cross-ketonization product or stearic acid were observed. From these experimental observations, it can be concluded that under the applied ketonization conditions, the liquid phase ketonization of fatty acids may be treated as an irreversible reaction. As a consequence, the following kinetic models exclusively include parameters related to the forward reaction.

### 3.3.5 Kinetic rate equation for liquid phase catalytic ketonization of fatty acids

A kinetic model was developed for both catalysts to gain further insight in the elemental steps of the liquid phase ketonization of fatty acids and its rate-determining step (RDS). Based on the good agreement of our activation energy data with previous kinetic studies on gas-phase ketonization, the bimolecular C-C coupling of two adsorbed carboxylic acid (derived) species is proposed as the RDS on the catalyst surface (eq. 8). Furthermore, all three reaction products are assumed to compete for the same active surface site (\*) (eq. 5-7). Therefore, the elementary reaction steps taken into account are adsorption and desorption of substrate and products, and the C-C coupling of two activated substrates on the catalyst surface:



As a result, a Langmuir-Hinshelwood (LH) kinetic model is obtained for the liquid phase ketonization reaction according to eq. 9 (see Supporting Information for derivation):

$$R = k \frac{K_{Acid}^2 C_{Acid}^2}{(1 + K_{Acid} C_{Acid} + K_{ketone} C_{ketone} + K_{H_2O} C_{H_2O} + K_{CO_2} C_{CO_2})^2} \quad (9)$$

with  $R$  the ketonization rate,  $k$  the rate constant of the surface reaction,  $K_x$  the equilibrium adsorption constants and  $C_x$  the liquid phase concentrations of acid, ketone, water and carbon dioxide. To determine the kinetic and thermodynamic  $k$  and  $K_i$  parameters, multiple non-linear regression was performed with XLSTAT software by Addinsoft[38] using a numerical iterative Levenberg-Marquardt algorithm to minimize the objective function (sum

of square of errors). An overview of the results is given in Table 3, showing that all parameters are significantly different from zero.

First, they indicate a large difference in rate constant between both materials, as the  $k$  value for R is more than six times higher compared to A (on surface area basis). This corroborates the substantially higher intrinsic activity of R for ketonization of fatty acids. Secondly, a different degree of interaction of reagent and products is evident for both catalysts, since the adsorption constants not only significantly differ in absolute value, but also in relative order (see also Supporting Information). For A, the adsorption constants decrease in the order  $\text{CO}_2 > \text{H}_2\text{O} = \text{acid} > \text{ketone}$ , whereas this series is altered to  $\text{CO}_2 > \text{H}_2\text{O} > \text{ketone} = \text{acid}$  for R  $\text{TiO}_2$ . These observations clearly underscore the different sorption behaviour of the  $\text{TiO}_2$  surfaces under similar conditions, indicating different (surroundings of) active sites on the A and R surfaces. Notably, the significantly higher adsorption constants of ketone,  $\text{H}_2\text{O}$  and  $\text{CO}_2$  on R are in good agreement with the product inhibition experiments. Stronger adsorption of these products on the active surface sites indeed lead to a stronger inhibition of the overall ketonization rate. It is thus apparent that the intrinsically higher conversion rate of R is simultaneously counteracted by its higher sensitivity to product inhibition by adsorption, which is less dominant for A.

Table 3: Parameter estimation for lauric acid ketonization based on the Langmuir–Hinshelwood fitting of the experimental data.

	Anatase (A)		Rutile (R)		P-value*
	Value	95% CI	Value	95% CI	
$k(\text{M}/\text{m}^2\text{h}) * 10^{-3}$	$1.3 \pm 0.06$	1.2,1.3	$8.1 \pm 0.001$	7.7,8.6	$< 1 * 10^{-5}$
$K_{\text{Acid}}(\text{M}^{-1})$	$19 \pm 2.7$	17,20	$70 \pm 19$	62,78	$< 1 * 10^{-5}$
$K_{\text{ketone}}(\text{M}^{-1})$	$3.6 \pm 1.2$	3.1,4.1	$76 \pm 24$	65,86	$< 1 * 10^{-5}$
$K_{\text{H}_2\text{O}}(\text{M}^{-1})$	$20 \pm 7.8$	17,24	$527 \pm 169$	454,599	$< 1 * 10^{-5}$
$K_{\text{CO}_2}(\text{M}^{-1})$	$32 \pm 7.2$	28,35	$1028 \pm 289$	905,1152	$< 1 * 10^{-5}$

\* 2 sample t-test

While the numerical results of Table 3 cannot be compared due to the lack of available literature data on liquid phase fatty acid ketonization, it is valuable to discuss the general concepts that came out our data in comparison with previous kinetic studies, carried out in the gas phase for short-chain acids. Adsorption constants have been reported for  $\text{C}_2\text{-C}_4$  acid ketonization on  $\text{Ru}/\text{TiO}_2$  (P25) in the presence of a  $\text{Cu}/\text{SiO}_2$  co-catalyst under  $\text{H}_2$  atmosphere at 275-335 °C.[25] For reaction of butyric acid at 335 °C, the adsorption constant values were 0.102, 0.051, 0.003 and 0.002  $\text{Torr}^{-1}$  for acid, ketone, water and carbon dioxide, respectively. Stated otherwise, the ratios of the K values of the products in relation to the substrate equalled 0.5, 0.03 and 0.02 for ketone, water and carbon dioxide, respectively. In our case, these relative values are 0.19, 1.1 and 1.7 for the A catalyst, and 1.1, 7.5 and 15 for R  $\text{TiO}_2$  (for same product order). Comparatively, the ketonization products seem to have a stronger binding tendency in the liquid-phase batch reaction, especially for the R catalyst. The high absolute values of the K parameters for  $\text{H}_2\text{O}$  and  $\text{CO}_2$  are related to the low absolute concentrations of these compounds in the liquid phase under ketonization reaction conditions.

With these LH parameters, parity plots were constructed for A and R in Figure 7. They present the correlation between the measured reaction rates (experimental work throughout this study) and the predicted ketonization rates, calculated based on the above developed LH model. In general, it can be stated that this kinetic model is in good agreement with the observed experimental results, while deviation is mostly observed for the higher H<sub>2</sub>O and CO<sub>2</sub> concentrations, especially for the R catalyst. Nevertheless, the kinetic model correlations are satisfactory, especially when considering the complexity of the system due to the difficulty of determining exact concentrations of water and carbon dioxide in the condensed phase where the catalysis is actually taking place. Furthermore, interaction between these products in the reaction liquid or on the catalyst surface may not be discarded yet (formation of bicarbonates for example). The margins of error/uncertainty on these parameters reflect this complex system, which we have studied in detail for the first time. Future research should expand on these topics, as well as further expand the set of reaction conditions.

Comparison of the kinetic equation with those reported for gas phase ketonisation reveals several differences. Some of these LH models completely exclude product inhibition, whereas others introduce separate adsorption of the carboxylic acid substrate and ketonization products on different types of active sites.[54] As stated in the introduction part, an ER mechanism has also been suggested for the aqueous phase ZrO<sub>2</sub> catalysed reaction of acetic acid.[33] In this ER mechanism, it is assumed that only one carboxylic acid is adsorbed and activated on the catalyst surface, which then directly undergoes the C-C coupling reaction with a second non-adsorbed carboxylic acid from the liquid phase. Such ER model cannot accurately describe our experimental results (Supporting information, Figure S10 and Table S3), and we have shown the rate determining step to be the C-C coupling of two adsorbed acid species.

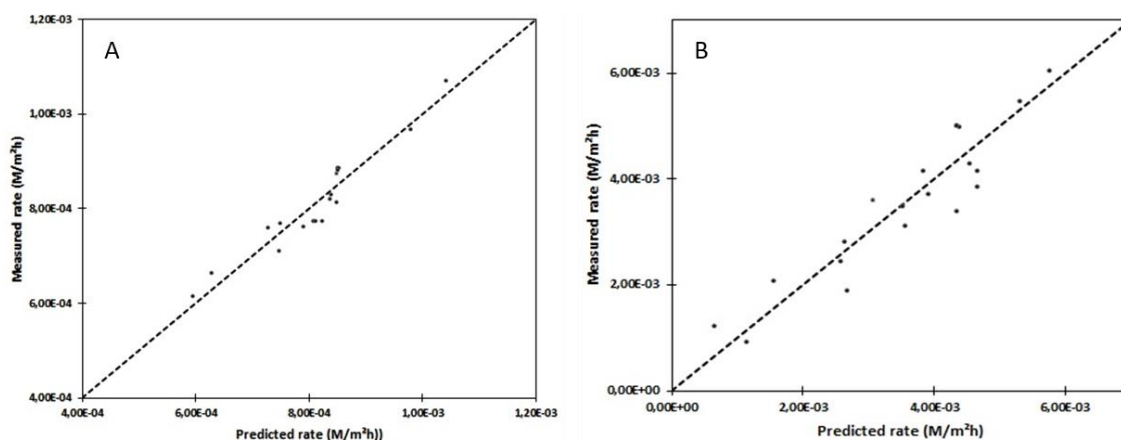


Figure 7: Parity plots displaying correlation between measured experimental ketonization rates and reaction rates as predicted by LH model (eq. 9) for A (A) and R (B) catalysts.

### 3.3.6 Ketonization activity of anatase (A) and rutile (R) TiO<sub>2</sub>

This kinetic study clearly indicates significant differences between A and R with regard to their conversion rate (type and number of active sites) and inhibition effects (sensitivity of the active sites). An earlier gas-phase study also revealed ketonization performance differences among these TiO<sub>2</sub> crystal phases, showing five times higher initial turnover rate of acetic acid for an anatase catalyst compared to the stronger acidic rutile TiO<sub>2</sub>. [13] These findings are opposite to our results, and were ascribed to two different factors. According to the authors, the specific crystal

lattice distances between active Ti-Ti and Ti-O species of anatase are more suitable for adsorption of acetic acid in monodentate configuration, which was proposed as the reactive substrate form to undergo C-C coupling. Secondly, TS experiences increased stabilization on anatase, due to the intermediate strength of Lewis acid-base sites. Oppositely, the smaller  $d_{\text{Ti5c-Ti5c}}$  of rutile results in a less favorable surface environment for the formation of TS, which is hindered sterically and stabilized less as a result of the stronger acidity of catalytic sites. Furthermore, acetic acid is preferentially adsorbed in bidentate mode on rutile, which was assumed to be a non-reactive spectator configuration. Interestingly and in sharp contrast, a very recent gas phase study found, as in our work, rutile  $\text{TiO}_2$  to be more active than anatase for ketonization of acetic and propionic acid.[55] Here, the shorter intermolecular separation of two adsorbed carboxylate substrates on rutile was used as primary reasoning to explain its higher ketonization activity. The same was also proposed earlier for the liquid-phase reaction of  $\text{C}_2$  acid, albeit with modified anatase and rutile  $\text{TiO}_2$  catalysts by incorporating Ru metal.[31] In the latter, the batch ketonization reaction was carried out in water and hexane solvents using bifunctional 5% Ru/ $\text{TiO}_2$  catalysts. The bifunctional rutile catalyst was characterized by a higher Lewis acid site density, a direct consequence of more favorable  $\text{TiO}_2$  surface reduction by the Ru metal via hydrogen spillover compared to the anatase catalyst. According to the authors, this increased amount of and shorter distance between active  $\text{Ti}^{3+}$  Lewis acid sites improved the acetic acid conversion rate in hexane by 150-400% compared to anatase. Additionally, incorporation of Ru can also impact the surface acid site strength, This will in turn influence adsorption and desorption of ketonization substrates, intermediates and products, impacting the ketonization rate.

It must be noted that in these literature examples the catalysts and reaction systems are not always identical, which could implicate that the catalytic behavior of different  $\text{TiO}_2$  materials is dissimilar in opposing systems. Clearly, our experimental and kinetic findings are more in line with the latter two studies, since the LH intrinsic rate constant  $k$  of the surface reaction is 6.4 times higher for R. Furthermore, the observed ketonization rate of lauric acid is 1.3 to 5.6 times higher on R, depending on how the reaction rate is expressed (Table 4). Therefore, our findings suggest that the higher Lewis acid site density, the smaller Ti-to-Ti distances or a combination of both are likely explanations for the higher reactivity of R  $\text{TiO}_2$  for liquid-phase fatty acid ketonization.

Table 4: Comparison of observed ketonization rates expressed as function of weight, surface area and acidity between A and R  $\text{TiO}_2$ . Reaction conditions: 15 mmol LA – 40 g DD – 0.3 g  $\text{TiO}_2$  – 340 °C - 45 min - 600 rpm – autogenous pressure.

Ketonization rate	Anatase (A)	Rutile (R)	R/A ratio
$R(g/g \cdot h)$	2.5	4.0	1.6
$R(M/m^2 \cdot h) * 10^{-4}$	9.0	50	5.6
$R(M/\mu\text{mol} \cdot h) * 10^{-4} (150\text{ }^\circ\text{C})$	7.4	29	3.9
$R(M/\mu\text{mol} \cdot h) * 10^{-4} (250\text{ }^\circ\text{C})$	8.6	18	2.1
$R(M/\mu\text{mol} \cdot h) * 10^{-4} (350\text{ }^\circ\text{C})$	20	21.5	1.3

### 3.3.7 Mechanism

As stated in the introduction, current literature on the ketonization reaction mechanism suggests a pathway via a  $\beta$ -ketoacid intermediate with the C-C coupling as RDS.[10] Furthermore, the presence of  $\alpha$ -H in one of the substrates

is required to observe any ketonization activity. This hydrogen atom is abstracted from the substrate by the active surface, leading to the formation of an adsorbed 1-hydroxy enolate species which can interact with a second adsorbed substrate molecule. [14] Both the kinetic and thermodynamic parameters obtained in our kinetic study ( $E_a$ ,  $\Delta H^\ddagger$ ,  $\Delta S^\ddagger$  and  $\Delta G^\ddagger$ ) are in good agreement with those obtained in earlier (mechanistic) work [13, 25], and our kinetic experimental data are consistent with the proposed Langmuir Hinshelwood C-C coupling model, allowing us to propose a  $\beta$ -ketoacid ketonization mechanism for liquid phase reaction of fatty acids, presented in Figure 8 for lauric acid as an example.

First, two lauric acid molecules are adsorbed and activated on the catalytic surface by formation of a 1-hydroxy enolate and second adsorbed molecule after elementary steps such as  $\alpha$ -H abstraction (a). Then, the rate-determining C-C coupling step occurs between the 1-hydroxy enolate and second adsorbed molecule, forming the  $\beta$ -ketoacid precursor (b). The latter undergoes elementary steps at the surface, resulting in the formation of the  $\beta$ -ketoacid intermediate and water is released from the surface as ketonization by-product (c). Ultimately, the intermediate dissociates, forming  $\text{CO}_2$  by-product and the primary ketone product (d). After ketone desorption, the catalytic cycle is complete.

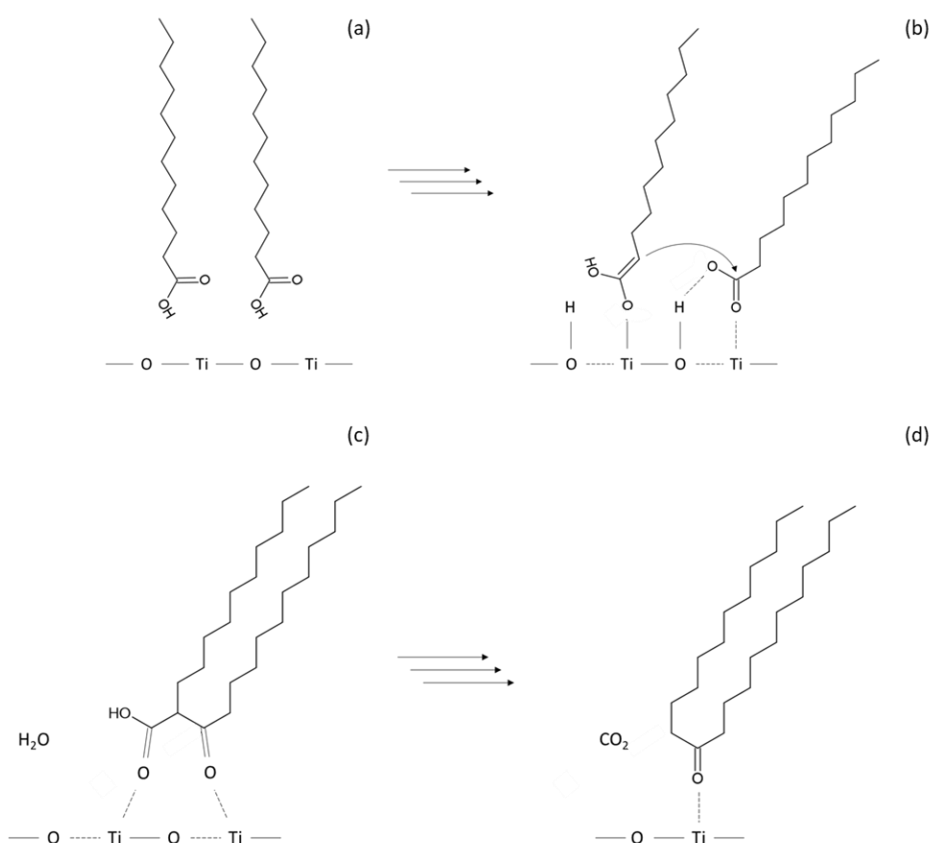


Figure 8: Proposed mechanism for lauric acid ketonization on  $\text{TiO}_2$  in liquid phase via  $\beta$ -ketoacid intermediate.

### 3.3.8 Effect of substrate chain length on ketonization rate

While lauric acid has been used as model compound up to this point, the influence of carbon chain length on the ketonization rate was also investigated by using saturated C<sub>14</sub>-C<sub>20</sub> fatty acid model compounds, namely myristic (C<sub>14:0</sub>), palmitic (C<sub>16:0</sub>), stearic (C<sub>18:0</sub>) and arachidic acid (C<sub>20:0</sub>). The same initial fatty acid loading of 15 mmol was used for all compounds, alongside identical reaction conditions, previously used for lauric acid. The results are summarized in Figure 9A. As depicted in the graph, the ketonization rate is clearly affected by the fatty acid chain length. Shorter fatty acids show higher activity, which holds true for both TiO<sub>2</sub> catalysts. This observation is in line with previously reported general trends on gas-phase carboxylic acid coupling.[2] Additionally, this relationship seems to follow a rather linear trend for both catalysts, though the absolute degree of reduction is larger for R. For instance, the observed reaction rates are reduced by 29 and 57% for stearic acid when compared to lauric acid, for A and R, respectively.

To uncover the origin of the reduced ketonization rate for the longer fatty acids in the liquid phase, the coupling reaction of stearic acid (C<sub>18:0</sub>) was carried out with the A catalyst at different temperatures between 300-340°C (Figure S11). From these data an apparent activation energy of 148 ± 13 kJ/mol was determined (Arrhenius equation), which is higher (but not statistically significant) than the 137 ± 7 kJ/mol value observed for lauric acid. Secondly, the observed enthalpy, entropy and Gibbs free energy of activation values were also calculated for stearic acid. The ΔH<sup>‡</sup>, ΔS<sup>‡</sup> and ΔG<sup>‡</sup> values were 143 ± 14 kJ/mol, -107 ± 26 J/mol.K and 208 ± 20 kJ/mol at 340 °C, respectively, for the rate determining step (C-C coupling). These means are all higher compared to lauric acid at the same reaction temperature, although further study including broader temperature ranges is necessary to more accurately determine the underlying cause of the observed differences (Table 5).

Assuming constant temperature independent values for ΔH<sup>‡</sup> and ΔS<sup>‡</sup>, ΔG<sup>‡</sup> values were plotted as a function of the reaction temperature between 300-550 °C (Figure S12A). For lauric acid, there is a common intercept for the A and R TiO<sub>2</sub> graphs at 500 °C, indicating that the ΔG<sup>‡</sup> value becomes lower for the A catalyst at > 500 °C. Similarly, the ΔG<sup>‡</sup> value of SA becomes lower than that of LA for the A catalyst at 470 °C (Figure S12B). For longer fatty acids, the

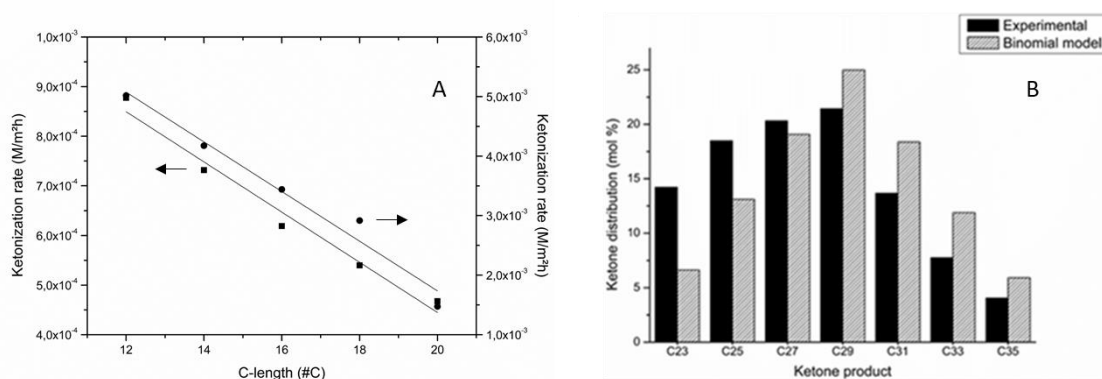


Figure 9: Ketonization rate in function of fatty acid substrate chain length for A (■) and R (●) TiO<sub>2</sub>. Reaction conditions: 15 mmol FFA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C - 45 min - 600 rpm – autogenous pressure (A). Experimental ketone product distribution after ketonization of an equimolar mixture of saturated C<sub>12</sub>-C<sub>18</sub> fatty acids in the presence of A TiO<sub>2</sub> vs. binomial model prediction. Reaction conditions: 15 mmol FFA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C - 45 min - 600 rpm – autogenous pressure (B).

TS is bulkier and likely subjected to more steric hindrance, negatively impacting the formation of the C-C bond (RDS). This increases the energy barrier for the C-C coupling, and therefore the enthalpy and Gibbs free energy of activation values. In the  $\beta$ -ketoacid ketonization mechanism, it is possible that the nucleophilic character of the  $\alpha$  C atom of the 1-hydroxy enolate is diminished by the stronger electron-donating properties of these longer alkyl chains, slowing down the RDS.[13] Regarding the entropy of activation, the higher entropy loss of shorter substrates may be a result of the general adsorption structure of the transition state during ketonization, as surface interaction occurs via the carbonyl groups. As this structure maintains rather similar for all substrates, the longer fatty acids have more carbon atom groups which are distanced further away from the catalyst surface, preserving a higher overall degree of freedom compared to carbon atoms of the shorter substrate chains, resulting in the lower entropy of activation (absolute value).[26] Although not yet conclusive, our results suggest that the more active R catalyst may also be more prone to the effect of increased steric hindrance for longer fatty acids compared to A.

Table 5: Summary of Arrhenius and Eyring-Polanyi model results for lauric and stearic acid ketonization on A TiO<sub>2</sub> at 340°C.

	Lauric acid		Stearic acid		P-value*
	Value	95% CI	Value	95% CI	
<b>E<sub>a,obs</sub> (kJ/mol)</b>	137 ± 7	129,145	148 ± 13	132,164	0.26
<b>ΔH<sup>‡</sup> (kJ/mol)</b>	132 ± 7	124,140	143 ± 14	127,159	0.29
<b>ΔS<sup>‡</sup> (J/mol.K)</b>	-121 ± 19	-99,-143	-107 ± 26	-76,-136	0.49
<b>ΔG<sup>‡</sup> (kJ/mol)</b>	206 ± 16	188,224	208 ± 20	185,231	0.89

\* 2 sample t-test

### 3.3.9 Fatty acid mixtures

Based on the findings of the previous section, and since biomass feedstock mainly consist of fatty acid mixtures, an equimolar mixture of saturated C<sub>12</sub>-C<sub>18</sub> fatty acids was used as ketonization substrate in the presence of the A catalyst. In this case, 7 different ketones can be formed with carbon chain lengths varying between 23 and 35 due to homo- and cross-ketonization of the 4 fatty acids. In Figure 9B, the ketone distribution of the obtained product mixture is displayed after a reaction time of 45 minutes, and compared to the predicted outcome when a binomial model is used to describe the product distribution. For the latter, it is assumed that the probability of ketonization between two fatty acid molecules on the catalyst surface is equal for all substrates. However, the experimental results clearly show an enrichment of lower MW ketones (C<sub>23</sub>-C<sub>27</sub>) compared to the binomial model, whereas the experimental yield of C<sub>29</sub>-C<sub>35</sub> is lower than predicted. These findings for fatty acid mixtures may be linked to the results of the previous paragraph, showing higher ketonization reactivity for lower MW fatty acids, which has been reported before for gas phase ketonization reactions of short-chain carboxylic acids.[2] For longer reaction times, the partial conversion values of the fatty acids will approach each other, since the lower MW substrates will be depleted faster in the beginning, clearing the catalyst surface for (slower) ketonization of the remaining longer fatty acid molecules (Figure S13).

### 3.3.10 Impact of solvent

Up until now, all experiments in this study were performed in the liquid phase with dodecane as inert reaction solvent. While not shown here, we observed identical reaction rates when dodecane was replaced by hexadecane, indicating that there was no impact of the hydrocarbon chain length and/or boiling point. Additionally, batch experiments were also performed with pure lauric acid substrate without any added solvent, to investigate whether this reaction system might influence our previously observed activity patterns. Hereto, similar reaction conditions (temperature, catalyst loading, stirring rate) were chosen under autogenous pressure, and 40 g lauric acid substrate (0.2 mol) was used to provide adequate loading in the 100 ml batch reactor. The results of these experiments are shown in Table 6 (entries 1-6) for times up to 6 hours (including heating phase) for both the A and R catalyst.

Table 6: Solvent and pure liquid phase ketonization of lauric acid with A and R catalysts in batch and semi-batch modes.

Entry	Solvent	Mode	Catalyst	t (min)*	X (%)
1	/	Batch	A	90	9.2
2	/	Batch	A	180	12
3	/	Batch	A	360	18
4	/	Batch	R	90	4.1
5	/	Batch	R	180	8.6
6	/	Batch	R	360	14
7	Dodecane	Batch	A	90	28
8	Dodecane	Semi-batch	A	90	40
9	Dodecane	Batch	R	90	53
10	Dodecane	Semi-batch	R	90	93
11	/	Semi-batch	A	90	14
12	/	Semi-batch	R	90	8.4

\*Including heating phase

Solvent reaction conditions: 15 mmol LA – 40 g DD – 0.3 g TiO<sub>2</sub> – 340 °C – 600 rpm. Pure reaction conditions: 0.2 mol LA – 4 g TiO<sub>2</sub> – 340 °C – 600 rpm. Batch experiments were conducted at autogenous pressure, semi-batch experiments were conducted at 10 bar with N<sub>2</sub> purging flow of 10 ml/min.

Similar to the solvent system, the ketonization selectivity was always very high ( $\geq 97\%$ ) for both catalysts. However, it is interesting to observe that here the A catalyst now shows a higher overall fatty acid conversion (and thus ketone yield) than R for all reaction times (entries 1-3 *versus* entries 4-6). This is opposed to our results of the solvent system, in which the R catalyst showed higher overall conversion of lauric acid. Furthermore, the absolute conversion values are much lower, with LA conversion values reaching 18% and 14% after 6 hours for A and R,



respectively. This indicates that the reaction rate is still higher for R when expressed on a surface area basis (by a factor of 1.5), as was the case for the solvent system (albeit it is now less pronounced). The activity patterns are clearly different for both reaction systems, which can be ascribed to the different reaction environment surrounding the catalyst and the substrate and product molecules. For the pure lauric acid system, the complexity rises even further than for the solvent system due to many (still) unknown factors such as solubility and concentrations of fatty acids, ketone, CO<sub>2</sub> and water in the intricate reaction medium. Related to this, it may also be linked to difference in sensitivity to product inhibition for both catalysts, as shown throughout this work for the solvent system. Since the R catalyst is more prone to product inhibition, potentially higher product concentrations at the catalytic surface could be a cause of the observed experimental results. To the best of our knowledge, this difference in activity patterns is reported for the first time in this work, while no other studies have compared or investigated these topics for (fatty acid) ketonization. Future research on this topic may also include the use of other solvents to investigate the potential influence of solvent properties on liquid phase fatty acid ketonization.

### 3.3.11 Impact of venting

Lastly, lauric acid ketonization experiments were performed in semi-batch operation mode to determine whether the decrease in catalytic activity due to product inhibition could be limited (or even mitigated completely). Hereto, the same reactor was used, but with the addition of a continuous in-and-out flow of the gas phase. This was achieved by purging N<sub>2</sub> through the liquid reaction medium at constant pressure via a gas inlet tube connected to the mechanical stirrer. At the reactor outlet, a condenser is maintained at 5°C, which prevents any liquid substrate or product loss. This implies continuous permanent removal of CO<sub>2</sub> and other gasses, while water, solvent, fatty acid and ketone are only temporarily removed (if applicable) as they are sent back into the reaction medium after contact with the condenser (and backflow to the reactor). Similar reaction conditions were used as before, with a constant pressure of 10 bar and a N<sub>2</sub> purging flow of 10 ml/min for the semi-batch experiments.

The results are shown in entries 7-12 of Table 6 for the A and R catalysts. Overall, they reveal a significant improvement of the conversion rate for both catalysts and reaction systems under semi-batch mode. For the solvent system, the conversion rate of lauric acid increased by 43% for the A catalyst (entries 7-8), while the R catalyst showed an even higher improvement of 75% (entries 9-10). These findings are in line with the difference in sensitivity to product inhibition for both catalysts, as it was shown before by our kinetic model that R is impacted more heavily by these phenomena. By continuous purging, the catalyst with the highest sensitivity showed the highest increase in catalytic activity. This trend is also present in the pure lauric acid liquid phase reactions, and to an even greater extent. Here, the ketonization rate of lauric acid increased by 48% for the A catalyst (entry 1 *versus* 11), while the R catalyst showed a remarkable improvement as the reaction rate was more than doubled (entry 4 *versus* 12). Clearly, removal of the reaction products is an efficient way to boost catalytic performance during liquid phase fatty acid ketonization.

## 4. Conclusions

In this work, the kinetics of liquid phase ketonization of C<sub>12</sub>-C<sub>18</sub> fatty acids over two TiO<sub>2</sub> catalysts, anatase and rutile, were studied for the first time. These high surface area catalysts, with Lewis acid-base amphoteric properties, both

showed high selectivity towards the ketone product. It was found that the R catalyst, with a higher Lewis acid site density, had a significantly higher intrinsic ketonization activity for lauric acid coupling compared to A, in addition to a lower observed activation energy. The observed reaction order values of lauric acid indicated a chemical regime in which the catalytic sites approach a state of substrate saturation for higher concentrations of fatty acid. Our kinetic experiments showed that the more active R catalyst was also more prone to product inhibition of water, ketone and carbon dioxide due to competitive adsorption of these reaction products on the active surface sites. This product inhibition becomes important for solvent-less reaction, for which A showed the highest overall conversion rate. We have proposed a strategy to counter this product inhibition by CO<sub>2</sub> (and partly water) via their continuous removal with inert gas purging, enabling drastic improvement of the conversion rates.

Based on our experimental findings, a kinetic LH model was developed for both catalysts. Besides highlighting the importance of adsorption/desorption of substrate and product molecules on the active surface, the kinetic models indicate that the C-C coupling elementary step is rate determining in the liquid phase ketonization reaction mechanism of fatty acids. The ketonization activity of the TiO<sub>2</sub> catalysts is likely determined by a combination of the Lewis acid site density and the crystal lattice distances between active Ti species. Related to the latter, steric effects could potentially negatively impact the C-C bond formation for the longer fatty acids, increasing the energy barrier for TS at the active surface. This lowers the ketonization reactivity of the longer substrates, which is more pronounced for the R catalyst, in line with its shorter Ti-to-Ti distances compared to A. As a result, shorter ketones are enriched in the product mixture at early stages of the reaction when starting from equimolar fatty acid substrate mixtures.

## Conflicts of interest

There are no conflicts of interest to declare.

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