# Measuring the performance of more circular complex product supply chains

3	Ellen Bracquené <sup>1</sup> , Wim Dewulf <sup>1</sup> , Joost R. Duflou <sup>1</sup>
4 5	1. KU Leuven, Departement of Mechanical Engineering, Celestijnenlaan 300A Box 2422, 3001 Leuven, Belgium
6	Contact info: ellen.bracquene@kuleuven.be
7	Keywords: circular economy; product circularity indicator; material efficiency; environmental trade-off;
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9	Abstract
10	This paper researches the possibility to measure the performance of more circular complex product supply
11	chains. Although a number of circularity indicators have already been proposed in literature, none was
12	found to properly describe the product system taking into account the 'tightness' of the material cycles
13	and the relationship with other product systems such as the use or supply of recycled material. Therefore,
14	a new Product Circularity Indictor (PCI) is developed in this paper. The ability of the PCI to overcome the

main limitations identified is demonstrated in a comparative study with the existing Material Circularity 15 16 Indicator (MCI). In addition, the new indicator is applied and tested in a case study for Washing Machines 17 (WM). The case study results show that the proposed PCI is a useful indicator to quantify the effectiveness 18 of different circular economy (CE) strategies. A shift to CE presents the challenge of recirculating material 19 flows in a manner that can promote eco-effectiveness. Therefore the potential trade-off between 20 increasing circularity and minimising the environmental burden of the WM is investigated using Life Cycle 21 Assessment (LCA) to quantify the potential environmental impact of the product system.

#### 1. Introduction 22

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23 The ambition to 'Live well within the limits of our planet' has guided policy-makers around the world to 24 define specific goals and action plans [1]–[3]. The limits of our planet are described in a comprehensive 25 manner by Rockström [4]. The planetary boundaries are defined for a wide range of environmental 26 processes that are affected by anthropogenic perturbations. However, the amount of resources that can be extracted without the risk of destabilizing the Earth System (ES) has not been defined. Natural 27 28 resources, although extracted from the environment, are a man-made concept and limitations from social 29 and environmental impacts are likely to result in economic scarcity well before physical depletion occurs 30 [5]–[7]. This explains the difficulty of assessing resource depletion as an environmental impact category 31 [8], [9] despite the growing concern for future limitation in terms of resource inputs and waste sinks [10].

32 It is widely recognized that the current linear supply chain based on a discard oriented society is not 33 sustainable and that there is a need for transition towards an economy that will decouple economic progress from resources depletion [11]–[13]. The Circular Economy (CE) concept summarizes different 34

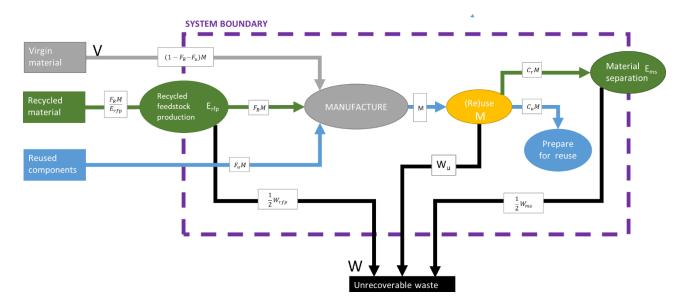
approaches that can contribute to this overarching goal [14]–[16]. A shift to circular economy presents the 1 2 challenge of recirculating material flows [17] in a manner that can promote eco-effectiveness [18]. 3 Different strategies exist for the restoration of material flows such as repair, preserving the product as a 4 whole, refurbishment, preserving the use of components or, as a last resort, recycling the material. The 5 strategies are complementary to each other because they act at a different stage of the product cycle. This 6 paper researches the possibility to measure the performance of more circular complex product supply 7 chains. In this context, circularity is defined as the ability to conserve both the quantity and the quality of 8 the material. The quality conservation can partially be described through the tightness of the material 9 circle which encourages to maintain products (and components) at their highest level of value for as long 10 as possible [19].

11 Several authors have investigated the definition and use of circularity measures [17], [20]–[28]. Circularity 12 can be assessed at different levels ranging between micro or product-level, meso or (inter)company-level 13 and macro or (inter)regional-level [29]. Macro-level indicators, generally based on Material Flow Analysis 14 (MFA), have been more widely applied and researched compared to micro-level indicators [10], [17], [30]-15 [32]. However, micro-level indicators are necessary to capture the effect of potential interventions at 16 product level where many CE strategies are put into practice. The three most commonly cited micro-level 17 indicators are the Material Circularity Indicator (MCI), proposed by the Ellen MacArthur Foundation (EMF) 18 and Granta Design (GD) [22], the Circular Economy Index (CEI) proposed by Di Maio and Rem [33] and the 19 Reuse Potential Indicator (RPI) proposed by Park and Chertow [34]. Linder et al. conclude the MCI is one 20 of the most promising and ambitious attempts yet to develop a product-level circularity metric [17]. In 21 their state of the art analysis of CE measures, Elia et al. also found that, at micro level, the proposed MCI 22 indicator managed to incorporate most of the desired CE requirements [35]. Garza-Reyes et al. also 23 considered the MCI to be the most complete assessment framework for micro-level circularity available in 24 literature [23]. Different authors have selected the MCI to measure the circularity at micro-level in their 25 analysis of the trade-off between material circularity and environmental efficiency [24], [36].

In this paper, the main limitations of the existing Material Circularity Indicator (MCI) are discussed and a new Product Circularity Indicator (PCI) is developed. The ability of the PCI to overcome the identified limitations is investigated in a comparative study with the MCI. In addition, the PCI is applied and tested in a case study for Washing Machines (WM). Finally, the potential trade-off between increasing circularity and minimising the environmental burden is investigated using Life Cycle Assessment (LCA).

# 31 **2. Method for circularity assessment at product level**

The objective of the Material Circularity Indicator (MCI) developed by EMF and GD is 'to measure the extent to which the linear flow has been minimized and restorative flow maximized' [22]. A summary of the equations used in the MCI mathematical model are given in Table 1 and a detailed description of their derivation is available in literature [22]. Figure 1 shows the system boundary of the MCI.



### 1 2

Figure 1: System boundary of the Material Circularity Indicator (MCI)

3 The product has a total mass (M) and is partly manufactured from virgin feedstock (V). A function (F) is derived depending on the utility (X) of the product in such a way that the MCI increases with improved 4 5 utility. The total mass W of unrecoverable waste that is attributed to the product system includes the 6 uncollected waste after use ( $W_u$ ), waste generated during material recovery ( $W_{ms}$ ) and recycled feedstock 7 production ( $W_{rfp}$ ). However, the authors only include half of the waste related to material recovery and 8 recycling motivated by the 50/50 allocation rule [22]. According to the 50/50 allocation rule, the burden 9 of shared processes are equally distributed between the previous and/or subsequent lifecycle of the product system studied. In the MCI, the production of recycled material and the recovery of material at 10 11 end-of-life (EoL) are considered shared processes.

12 The MCI aims to quantify the fraction of material flows that are circular or non-linear compared to a linear 13 system. For a product with mass M, in case of a fully linear system, a mass M of material flows in the 14 system and another mass M flows out at end-of-life. This would result in a denominator of 2M. However, due to the 50/50 allocation, it should be corrected for the amount of waste generated by the recycled 15 feedstock production upstream allocated to the product system  $\left(\frac{W_{rfp}}{2}\right)$ . In addition, part of the waste 16 generated by the material recovery at EoL is allocated to the subsequent product system using the recycled 17 material  $\left(\frac{W_{ms}}{2}\right)$ . The MCI calculation method is therefore summarized by the following equations for the 18 19 Linear Flow Index (LFI) and the Material Circularity Indicator (MCI):

20 
$$LFI = \frac{V + W_u + \frac{W_{rfp}}{2} + \frac{W_{ms}}{2}}{2M + \frac{W_{rfp}}{2} - \frac{W_{ms}}{2}} (1)$$

$$MCI = 1 - LFI \cdot F(X) \quad (2)$$

Although the MCI allows for reused components ( $F_u$ ) to enter the value chain, this flow does not displace new manufactured components. In the MCI model, only one manufacturing stage is defined which includes all production activities simultaneously (material production, component production and assembly). As a
 consequence, the reused components are assumed to displace virgin material. In addition, the MCI

- 3 assumes that the flow of reused components and recycled material are fully circular, even though for some
- 4 flows only partial circularity can be accounted for within the considered product system. In order to be
- 5 fully circular, both the generation and the use of restorative flows must be demonstrated.

6 A first consequence of these assumptions and modelling choices is that the MCI is unable to account for 7 the 'tightness' of the material cycles (reuse vs. recycling) which can potentially have significant implication 8 for the effectiveness of the material cycling [17]. Secondly, the MCI completely ignores where the reused 9 components and recycled materials are sourced from and where the recovered components and materials will end up. Disregarding the relationship with other product systems, that absorb or generate recycled 10 11 feedstock, can only be motivated if the recovered material is reused within the system boundary. In order 12 to adequately describe a real-life open-loop product system, the exchange of components and recycled 13 feedstock with other product systems has to be taken into account because as long as the loop is not fully

14 closed it should not be accounted as such in the circularity metric.

15 In addition, the MCI does not take into account the effect of downcycling which can happen when the

16 material degrades due to changes in inherent properties. In this case the material can no longer be used

17 in the same or similar application. If downcycling is not incorporated in the circularity indicator, it is not

18 able to account for the quality preservation of recovered and recycled materials.

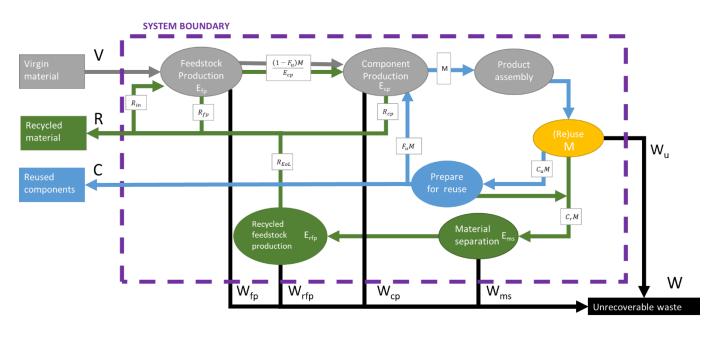
- Another limitation of the MCI is that only the recycled feedstock production is included while the other manufacturing stages, such as virgin feedstock production, are excluded in the main part of the methodology without any clear motivation. A first observation is that it would be more consistent to either include all or none of the manufacturing stages. In addition, even if only part of the manufacturing steps
- are included, the same cut-off should apply to both virgin and recycled material.
- Finally, the fraction of recycled material content  $(F_{rc})$  and fraction of reused components  $(F_u)$  are both defined at product or component level and are therefore not completely independent in the MCI model  $(F_{rc} + F_u \le 1)$ . In reality feedstock is produced from a mix of virgin and recycled material and it would therefore be more practical to define the recycled content  $(F_r)$  at material rather than at component or product level.

29 In this paper a novel method for circularity assessment at product level (PCI) is introduced to overcome 30 the main limitations identified for the existing indicator (MCI). The different manufacturing steps are considered and the associated material losses are accounted for as waste or recycled material. The 31 32 inclusion of separate manufacturing steps allows for the different restorative flows to re-enter the 33 production chain at the appropriate stage. The components harvested for reuse are assumed to avoid the 34 production of new components while the recovered and recycled materials are assumed to reduce the 35 need for virgin material. The feedstock production starts with the material processing step that includes 36 both virgin and recycled material as input, such as ingot production for metals. Potential losses during the 37 assembly stage are not included in the current PCI model.

The material separation and recycled feedstock production are fully part of our product system which 1 2 allows for clear boundary between product systems. However, in order to ensure mass balance, an 3 exchange with a stock of 'recycled material' is included. If the product system produces more recycled 4 material than it takes up, the surplus material will leave the system and will be added to the recycled 5 material stock. If, on the other hand, the product does not recover sufficient recycled material after the 6 use phase, recycled feedstock from the stock will be used as recycled content for the feedstock production. 7 The same reasoning can be applied to components. However, most components are product specific and 8 the exchange with other systems might not be practically feasible, expect for standardized components.

9 Figure 2 illustrates the model used to develop the PCI as described in this section of the paper. The

- 10 equations to calculate the necessary material flows are derived in the next subchapters and summarized
- 11 in Table 1.



- 12
- 13

Figure 2: System boundary of the Product Circularity Indicator (PCI)

### 14 2.1. Virgin material (V)

The amount of required virgin material is derived from the known mass of the final product (M). First, the fraction of reused components ( $F_u$ ) is deducted. Secondly, the production losses during component production and feedstock production are taken in account.  $E_{cp}$  and  $E_{fp}$  are the efficiency of the component and feedstock production. The manufacturing efficiencies determine the amount of material required upstream to cope with the subsequent losses down the supply chain. Finally, the amount of recycled content ( $F_r$ ) of the produced feedstock is deducted to calculate the amount of virgin material (V):

21 
$$V = \frac{(1 - F_u)M}{E_{cp} \cdot E_{fp}} (1 - F_r) \quad (1)$$

#### 1 2.2. Unrecoverable waste (W)

W is the total amount of unrecoverable waste leaving the product system. The PCI model includes both manufacturing waste and post-use waste. Manufacturing waste includes waste from feedstock production  $(W_{fp})$  and waste from component production  $(W_{cp})$ . However not all material loss during production is waste.  $C_{fp}$  and  $C_{cp}$  are the fractions of material losses that are recovered as useful recycled material. The manufacturing waste generated is calculated with the following equations taking into account the efficiency of the feedstock production  $(E_{fp})$  and of the component production  $(E_{cp})$ :

8 
$$W_{fp} = \frac{(1 - F_u)M}{E_{fp}E_{cp}} (1 - E_{fp}) (1 - C_{fp})$$
(2)

9 
$$W_{cp} = \frac{(1 - F_u)M}{E_{cp}} (1 - E_{cp})(1 - C_{cp}) (3)$$

10 The post-use waste includes the material sent to energy recovery or landfill at end-of-use ( $W_u$ ), waste 11 generated during material separation ( $W_{ms}$ ) and waste generated during recycled feedstock production

12 (W<sub>rfp</sub>). These waste streams can be calculated as follows:

13 
$$W_u = M(1 - C_u - C_r)$$
 (4)

14 
$$W_{ms} = M (1 - E_{ms})C_r$$
 (5)

15 
$$W_{rfp} = ME_{ms}C_r \left(1 - E_{rfp}\right)$$
(6)

16  $C_u$  represents the fraction of collected end-of-use products available for component reuse. Even though a 17 product is collected for reuse, it is most likely not feasible to reuse all components.  $C_r$  represents the 18 fraction that is collected for recycling. The recycling consists of two distinct steps: material separation at 19 end-of-life for resource recovery and further material processing to produce usable recycled feedstock. 20 Efficiency factor  $E_{ms}$  is the efficiency of the material separation and  $E_{rfp}$  is the efficiency of the recycling 21 process used to produce the recycled feedstock.

22 The total unrecoverable waste W can be calculated as follows:

23

 $W = W_{fp} + W_{cp} + W_u + W_{ms} + W_{rfp}$ (7)

#### 24 2.3. Recycled material (R)

25 In many cases the amount of recycled material generated by a product system does not match the amount of recycled material used in the manufacturing stage of the same system. Furthermore, the recovered 26 27 material can often not be used for the same purpose due to quality losses with cascade recycling or 28 downcycling as consequence. In most product lifecycles, there is either a recycled feedstock shortage or 29 surplus. In the first case, recycled feedstock needs to be sourced from outside the product system. In the 30 latter case the generated feedstock should be used outside the product system under investigation. The 31 amount of recycled feedstock exchanged with the outer system (R) depends on the amount of recycled 32 material used as input  $(R_{in})$ , the amount of scrap generated during feedstock production  $(R_{fp})$  and component production ( $R_{cp}$ ), and the amount of end-of-life recycled material recovered ( $R_{EoL}$ ): 33

1 
$$R_{in} = F_r \frac{(1 - F_u)M}{E_{fp}E_{cp}}$$
 (8)

2 
$$R_{fp} = (1 - E_{fp})C_{fp}\frac{(1 - F_u)M}{E_{fp}E_{cp}}$$
(9)

3 
$$R_{cp} = (1 - E_{cp})C_{cp}\frac{(1 - F_u)M}{E_{cp}} \quad (10)$$

$$S R_{out} = R_{fp} + R_{cp} + R_{EoL} (12)$$

$$6 R = R_{in} - R_{out} (13)$$

Products can be collected for part harvesting to enable remanufacturing or repair. If the number of parts
recovered exactly matches the number of parts used, there is no exchange across the system boundary.
In other cases, the amount of material flowing through the system boundary for component reuse is
calculated as follows:

 $C = M(F_u - C_u) \qquad (14)$ 

13 When collected parts can no longer be (re)used, they are assumed to be recycled.

### 14 2.5. Utility factor (X)

The utility factor aims to take into account how durable products are manufactured on the one hand and how intensively they are used on the other hand. The first part is mostly depending on the design and manufacturing stage. In other words, the "use potential" of a products depends on the manufacturer, but the final "used potential" depends on the user.

19 The reliability requirements for products are set by engineers in the manufacturing industry. These 20 requirements determine the probabilistic need of satisfying specific product performance parameters 21 across the product life cycle. The design life of a product  $(L_d)$  is the period of time during which that 22 product system is expected by its designers to perform intended functions within its specified design 23 parameters and operational environment [37]. The design life is usually derived from the expected product 24 life by the customers in their viewpoint and time scales such as years. After the expected design life is 25 estimated based on market research, the design life in engineering terms or functional usage duty cycles 26  $(FUDC_d)$  can be calculated by assuming a specific use intensity  $(I_d)$  as design target. The product utility X 27 is defined as the ratio of the available or used FUDC versus the expected  $FUDC_d$  based on average 28 product design requirements:

29 
$$X = \left(\frac{L}{L_d}\right) \left(\frac{I}{I_d}\right) = \frac{FUDC}{FUDC_d} = \frac{Available or used functional units}{Expected functional units}$$
(15)

1 The denominator equals the number of functional units the product is designed to last for based on market average for a specific product group  $(FUDC_d)$ . The numerator represents the actual available or used 2 3 functional unit depending on the perspective of the assessment. The manufacturer can increase the 4 number of available functional units by designing a product for improved durability compared to market 5 average  $(FUDC > FUDC_d)$ . Due to the difficulty to measure actual reliability of products put on the 6 market, the available functional units can be based on the actual offering of the manufacturers which is 7 the warranty period. The manufacturer will maximize the product reliability within this timeframe to 8 minimize the warranty cost [38]. The consumer can increase the number of actual used functional units 9 by increasing the use intensity (e.g. product sharing). The actual used functional units by the customers 10 can be derived from consumer studies.

#### 11 2.6. Linear flow index (LFI)

12 The Linear Flow Index (*LFI*) is the fraction of material flowing through the system boundary in a linear 13 fashion compared to the fully linear systems. The amount of material flowing in and out a fully linear 14 system ( $F_r = F_u = C_u = 0$ ), is computed as follows:

15 
$$V_{linear} = W_{linear} = \frac{M}{E_{cp} \cdot E_{fp}}$$
(16)

16 The *LFI* can then be computed as follows:

17 
$$LFI = \frac{V + W + \frac{1}{2}|R| + \frac{1}{2}|C|}{V_{linear} + W_{linear}} \quad (17)$$

18 The recycled material and reused components, that are exchanged with other product systems, are in 19 between a linear and circular flow. They do not count as linear flow because of their potential to be reused 20 nor as fully circular because they depend on other product systems for either the generation or the use of 21 the recycled material and reused components. If downcycling is not acknowledged, it does not stimulate 22 the production of high quality secondary material and this could lead to accelerated degradation of the 23 recycled material pool [39], [40]. Product systems generating recycled material or reused components 24 should be rewarded for providing high quality material. On the other hand product systems using recycled 25 or reused material should be rewarded for using low grade material. Although downcycling should not be 26 encouraged, low grade application can broaden the possibilities for recycled feedstock when it is not 27 possible to avoid quality degradation. If a quality factor (Q) can be quantified that represents to what 28 extent the inherent properties of the material are lost, the following equation could be used:

29 
$$LFI = \frac{V + W + Q_{in}R_{in} - Q_{out}R_{out}}{V_{linear} + W_{linear}}$$
(18)

30  $R_{in}$  and  $R_{out}$  can be calculated using equations 8-12.  $Q_{in}$  and  $Q_{out}$  are the quality factor of the material 31 entering and leaving the product system respectively. The quality factor should be defined between [0,1] 32 with Q = 1 representing a quality undistinguishable from virgin material.

### 1 2.7. **Product Circularity Indicator (PCI)**

- 2 The PCI is calculated by considering the LFI and the utility X of the product in the following equation:
- $3 PCI = 1 \frac{LFI}{X} (19)$
- For products with a low utility (X < 1), the overall PCI computed with equation 19 can be a negative value.
- 5 For this reason the rule is added that if the PCI calculation turns negative, the PCI score is set equal to zero.

#### 6 2.8. Multi-material products

7 The PCI can be applied to a multi-material product using a mass-based weighting methodology:

8 
$$PCI_{total} = \frac{\sum_{i} M_{i} \times PCI_{i}}{\sum_{i} M_{i}} \qquad (20)$$

9 Equation 20 could also be used to calculate the individual PCI of each component. Lonca et al. have

10 demonstrated that such a disaggregation at component level would lead to minor deviations in the final

11 results at product level [24].

# 3. Comparison of new and existing circularity indicator

Table 1 provides an overview of the equations used in current proposed PCI calculation method. For easy
 comparison and to highlight the differences, the equations of the existing MCI method are included using
 a uniform symbol notation. The main differences between the PCI and MCI can be summarized as follows:

- 5 The recycled content  $(F_r)$  is defined at material level in the PCI, while, in the MCI, it is defined at 6 product level  $(F_{rc})$ .
- 7 8

9

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- Material losses during feedstock and component production are considered in the PCI. As a consequence, direct component reuse has more benefits compared to material recycling. This is a significant difference with the MCI method that only takes recycling efficiency into account.
- In the PCI, material recovery and material recycling are considered to be fully part of the product
   system.
  - Material flow exchanges with the outer system boundaries (R and C) are not accounted as fully circular in the PCI calculation method.

Parameter	Product Circularity Indicator	Material Circularity Indicator [22]	
Virgin material	$V = \frac{(1-F_u)M}{E_{cp}\cdot E_{fp}} (1-F_r)$	$V = M(1 - F_u - F_{rc})$	
Waste from feedstock production	$W_{fp} = \frac{(1 - F_u)M}{E_{fp}E_{cp}} (1 - E_{fP}) (1 - C_{fp})$	-	
Waste from component production	$W_{cp} = \frac{(1 - F_u)M}{E_{cp}} E_{fp} (1 - E_{cp}) (1 - C_{cp})$	-	
Uncollected EoL product	$W_u = M(1 - C_r - C_u)$	$W_u = M(1 - C_r - C_u)$	
Waste from material separation	$W_{ms} = M \ (1 - E_{ms})C_r$	$W_{ms} = M (1 - E_{ms})C_r$	
Waste from recycled feedstock production	$W_{rfp} = M E_{ms} C_R \left( 1 - E_{rfp} \right)$	$\frac{1}{2}W_{rfp} = M\frac{(1-E_{rfp})F_r}{E_{rfp}}$	
Unrecoverable waste	$W = W_{fp} + W_{cp} + W_u + W_{ms} + W_{rfp}$	$W = W_u + \frac{(W_{ms} + W_{rfp})}{2}$	
Recycled material used for feedstock production	$R_{in} = F_r \frac{(1 - F_u)M}{E_{fp}E_{cp}}$	-	
Recycled material recovered	$R_{out} = (1 - E_{fp})C_{fp} \frac{(1 - F_u)M}{E_{fp}E_{cp}} + (1 - E_{cp})C_{cp} \frac{M}{E_{cp}} + E_{rfp}E_{ms}C_rM$	-	
Recycled material (net exchange)	$R =  R_{in} - R_{out} $	-	
Reused components (net exchange)	$C =  M(F_u - C_u) $	-	
Linear Flow Index	$LFI = \frac{V + W + \frac{1}{2} R  + \frac{1}{2} C }{V_{linear} + W_{linear}}$	$LFI = \frac{V + W}{2M + \frac{Wrfp - Wms}{2}}$	
Utility factor	$X = \left(\frac{L}{L_d}\right) \left(\frac{I}{L_d}\right) = \frac{U}{U_d}$	$X = \left(\frac{L}{L_d}\right) \left(\frac{U}{U_d}\right)$	
Circularity Indicator	$PCI = 1 - \frac{LFI}{x}$	$MCI = 1 - 0.9 \frac{LFI}{x}$	

#### 14 Table 1: Overview of equations used in PCI and MCI calculation models

A sensitivity analysis is performed on a simple theoretical case to demonstrate the ability of the new PCI to overcome the identified limitation of the existing MCI. We assume a single material product with a fraction of components ( $F_u$ ) that can be reused. The material feedstock is partly produced from recycled material ( $F_r$ ). For the MCI calculations, we have to compute the recycled content at product level ( $F_{rc}$ ) with the following formula:

6

$$F_{rc} = (1 - F_u) * F_r$$
 (22)

7 We further assume that all products are collected ( $C_r = 1 - C_u$ ) and a closed loop for the components 8 ( $C_u = F_u$ ). The efficiency of all the processes is assumed to be to 0.85.

9 Figure 3 (a) and Figure 3 (b) show the sensitivity of both PCI and MCI with a change of product reuse  $(F_u)$ 

and recycled content of the material ( $F_r$ ). The results show that the PCI is much more sensitive to  $F_u$  thus

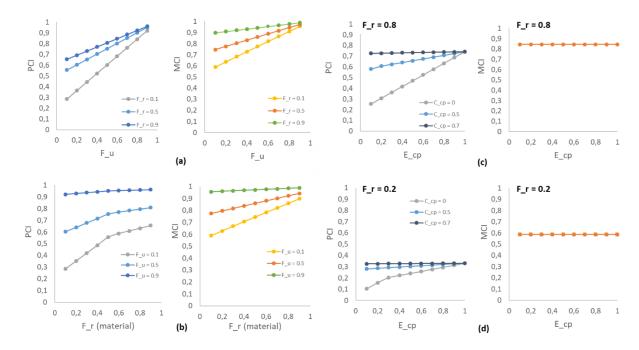
11 increasing the ability to reflect the tightness of the material cycle. In addition, the PCI behaves differently

12 for the same increase in recycled content depending on the exchange with other product systems for the

13 provision or absorption of recycled material. As long as the demand for recycled content is more than

supplied  $(R_{in} > R_{out})$ , an increase of  $F_r$  will result in a higher increase of PCI. Once  $R_{out} = R_{in}$  the slope

15 of the curve changes and the sensitivity of PCI as a function of  $F_r$  is reduced.





17Figure 3: Comparison between new PCI and existing MCI for a change in (a) fraction of reused components  $(F_u)$ , (b) recycled18content of material  $(F_r)$ , (c) component production efficiency  $(E_{cp})$  for high recycled content (d) component production19efficiency  $(E_{cp})$  for low recycled content

Further analysis is done to demonstrate the added value of incorporating a more detailed material flow during the production stage. For this analysis, the components of the single material product are assumed not to be reused ( $F_u = C_u = 0$ ). In addition, the product is assumed to be collected for recycling at endof-use ( $C_r = 1$ ). The efficiencies of the waste treatment steps are assumed to be 0.85 ( $E_{ms} = E_{prf} =$ 

24 0.85). For simplicity, only the efficiency of the component production  $(E_{cp})$  is varied while the efficiency

- 1 of the feedstock production is not taken into account ( $E_{fp} = 1$ ). Two different cases are considered. The
- 2 first assumes the product is made from feedstock with a high recycled content ( $F_r = 0.8$ ) and the second
- assumes low recycled content ( $F_r = 0.2$ ). For each case, the fraction of recycled material recovered during
- 4 manufacturing  $(C_{cp})$  is varied from 0 to 0.7.
- Figure 3 (c) and Figure 3 (d) show the sensitivity of the PCI with a change in manufacturing efficiency ( $E_{cp}$ ) for high and low recycled content. The influence of  $E_{cp}$  is more important for products made from materials with a high recycled content. On the other hand, the influence is minimized as more material loss during production is recovered for recycling ( $C_{cp}$ ). As expected, the MCI is not affected by this parameter and remains the same independently of  $E_{cp}$ . Even with a low recycled content ( $F_r = 0.2$ ), the MCI is relatively high. This is due to the surplus of recovered 'recyclable' material at end-of-life ( $C_r = 1$ ) that is assumed to be fully circular in the MCI model. In future, as collection rates are improved, a more
- 12 detailed micro-level circularity calculation method, such as the PCI, will become increasingly relevant to
- 13 allow differentiation between product systems.

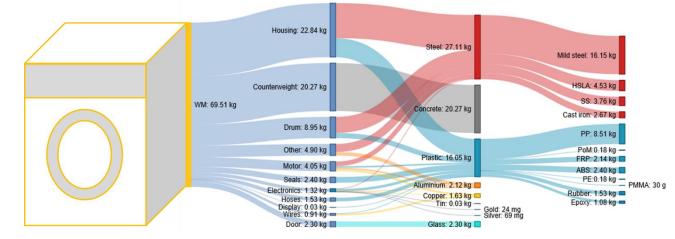
# 1 4. Case study: Washing machine (WM)

In this section, the developed PCI is applied to a real-life case study. The purpose is to demonstrate the practicability of the indicator and, in addition, to show the ability to investigate a number of improvement strategies based on CE thinking. WMs have a longer technological cycles which makes them a relevant candidate for CE strategies such as reuse and refurbishment. In previous research, WMs are often taken as an example to investigate eco-design measures such as durability [41], [42], repairability [43]–[45] or eco-efficiency [46]–[48].

## 8 4.1. Data collection

#### 9 Bill of Material

10 A summary of all the materials used in a WM and their respective weight is given in Figure 4. This summary is based on the Bill of Materials (BOM) received from a manufacturer. The total weight of the WM is 11 69.51 kg excluding packaging. The received dataset contains detailed information for the contribution of 12 13 each plastics type, but not for the type of steel used or for the exact composition of the electronic parts which include precious metals. Literature data are used to fill these data gaps. Ashby et al. reported that 14 59.9% (w/w) of the steel parts from a WM were manufactured from mild steel, 16.2% from High Strength 15 16 Low Alloy (HSLA) steel, 14% from stainless steel (SS) and 9.9% from cast iron [49]. The printed wiring board 17 (PWB) composition is estimated based on data from Oguchi et al. [50]. In this study a number of PWBs from different product types are analysed and the concentration of different elements is determined. 18 Based on this concentration and the known weight of the PWB in the WM, the amount of the different 19 20 (precious) metals is calculated.



- 21
- 22

Figure 4: Composition of the case study washing machine

#### 23 Recycled content of feedstock

24 The recycled content is defined as a material property. Average industry data is retrieved from literature

for each material type. Ashby et al have determined the recycled content per steel type [49]. The recycled

26 content of cast iron is around 69% while the HSLA steel is assumed not to contain recycled steel. Mild steel

- 27 and stainless steel have an average recycled content of 42% and 38% respectively. For concrete, Cullen et
- al. estimate a recycled content of only 2% [20]. Kaweki et al. have done a probabilistic material flow

analysis (MFA) for several plastic commodities in Europe [51]. For Polypropylene (PP), which is the most 1 2 commonly used plastic in WMs, the recycled content is estimated to be around 12% assuming all recovered 3 PP is reused as feedstock. Considering the numerous challenges to overcome, from separating the 4 different polymer fractions during waste treatment to ensuring sufficient quality of the recycled feedstock, 5 this is an optimistic assumption for the WM. Collecting meaningful and comprehensive recycling statistics 6 has proven very difficult for the aluminium industry because there are numerous remelting and refining 7 plants worldwide which can switch from scrap-based to primary-based production depending on market 8 prices and product requirements at any time [52]. Nevertheless, the dynamic material flow model 9 presented by Bertram et al. estimates that the global recycled content of aluminium is 52.6%. Based on 10 the dynamic model of global copper stocks and flows presented by Glöser et al., overall recycled content 11 is calculated and equals 35.31% [53]. Eventhough the use of recycled cullets in glass production can 12 amount to 50% of the material input, the glass used in electrical appliances is a specialty commodity 13 representing only 2% of the glass sector [54]. Due to its small size and specific application, no recycled 14 content is assumed for the glass used in the WM.

#### 15 Manufacturing losses

- 16 The manufacturing of products includes feedstock production and component production. For the metal
- 17 materials, the feedstock production starts with the ingot production and delivers half-fabricates. Table 2
- summarize the manufacturing efficiencies for feedstock production  $(E_{fp})$  and component production  $(E_{cp})$
- 19 based on the available literature. In addition, the fraction of material loss recovered for recycling is also
- 20 retrieved from literature when relevant for feedstock production  $(C_{fp})$  and for component production
- 21 (*C<sub>cp</sub>*).

Material type	E <sub>fp</sub>	C <sub>fp</sub>	E <sub>cp</sub>	C <sub>cp</sub>	Reference
Steel	73.95%	43.35%	87%	99%	[55]
Concrete	99%	-	99%	-	-
Plastic	100%	-	99.5%	-	[51], [56]
Aluminium	70.5%	95%	78%	96.8%	[57]
Copper	95.5%	0%	75%	100%	[53]
Glass	97%	-	97%	-	_

#### 22 Table 2: Overview of average manufacturing efficiencies based on literature values for global production

23

#### 24 Utility

Rüdenauer et al. have compared the use information for WM based on data received from the manufacturer [48]. Back in 1991, a manufacturer has designed his products to last for 3500 wash cycles (14 years x 250 washes/year). Ten years later, in 2001, the design life decreased slightly to 3135 wash cycles (15 years x 209 washes/year). Nowadays, 2500 wash cycles is a commonly assumed design life ( $U_d$ ) in industry (10 years x 250 washes/year) [21], [37], [41], [58]. These data suggest that the design life has

- 30 decreased with 28% over the last three decades.
- 31 Chen et al. analysed real life warranty data from a Chinese manufacturer, revealing that 3% of the sold
- 32 WM failed within the first 3 years and 50% failed within 13.6 years [38]. Unfortunately, the use intensity
- 33 of the devices was not monitored. Accelerated life tests (ALT) represent a methodology able to investigate

- 1 product reliability performance in a shorter time compared to the conventional standard testing methods,
- 2 both in the design and in the production phase. Based on such experiments, a reliability of 99.2% for 500
- 3 cycles and 89.78% for 1250 cycles at normal user condition was derived by Borgia et al. [21], [58] which
- 4 indicates that the product has a high reliability (>99%) in the first 2 years.
- 5 In most regions, household appliances are sold with a warranty period. Even though in some countries a 6 legally binding minimum is applicable, some manufacturers offer an extended warranty period for the
- 7 product or for a number of components. The technical call rate (TCR) for electronic products, defined as
- 8 share of products that fail during the warranty period, is often targeted to remain below 3% by internal
- 9 company policies [43]. This means that products are often designed for a reliability of 97% within the given
- 10 warranty period. For WM, 3 additional years are common practice [42]. Together with the legal minimum,
- 11 this usually results in a total of 5 years which covers 50% of the design life.
- 12 The actual consumer behaviour with respect to WM has been analysed at the University of Bonn. This
- 13 study found that the average number of washing cycle per year in Europe is decreasing due to smaller
- 14 household size and higher load per wash cycle [59]. The results varied significantly per household size with
- 15 2.2 cycles per week for a single person household and 6.8 for a household with at least five persons [59].
- Boyano et al. estimate an average lifespan of 12.5 years for WMs for an normal use (220 wash cycle per year) [60].
- 18 Table 3 provides an overview of the derived utility factors. For the baseline, a default utility (*X*) of 1 is 19 assumed.

Perspecticve	Lifetime (Years)	Intensity (Washes/year)	X (-)	Reference
Manufacturer – default warranty	2	250	0.2	-
Manufacturer – extended warranty	5	250	0.5	[42]
Baseline assumption	10	250	1	[41]
Consumer – average	12.5	220	1.1	[60]

#### 20 Table 3: Overview of derived utility factors

#### 21

#### 22 Refurbishment and component reuse

- Consumer repair and reuse is included in the previous section on utility and is therefore not considered
   here. This section is about the reuse of components or refurbishment performed by a professional reuse
   centre or by a manufacturing company. The latter would require a take-back scheme or a product as a
- 26 service business model.
- In Europe, the number of Product Service Systems (PSS) is increasing and Bluemovement is an example of
  such an initiative in the Netherlands<sup>1</sup>. It is founded by a WM manufacturer and allows customers to
  subscribe to the use of a WM rather than owning a WM. The customer can choose between a refurbished
  WM at less than 10 Euro/month and a new WM for a monthly subscription between 15 and 20 Euro/month

<sup>&</sup>lt;sup>1</sup><u>https://www.bluemovement.nl/abonnementen</u>

- 1 depending on the product features. The maximum duration of the subscription is however limited to 6
- 2 years. After this period the WM is refurbished or recycled.
- Currently such PSS schemes are not common practice and in the baseline scenario no refurbishment or
   component reuse is assumed. In the sensitivity analysis, however, a PSS scenario is investigated

#### 5 Collection at end-of-use

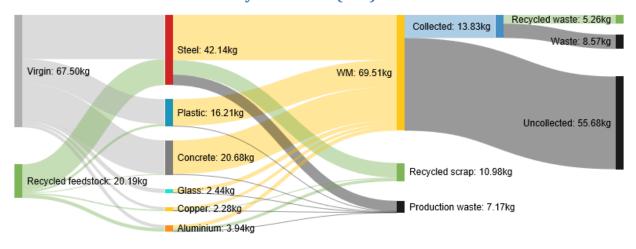
- 6 Waste of electrical and electronic equipment (e-waste) is a fast-growing waste stream with complex
- 7 characteristics. Rapid technology innovation and shortening product lifespans are among the factors
- 8 contributing to the growing amount of e-waste [61]. Globally, only 8.9 Mt of e-waste are documented to
- 9 be collected and recycled, which corresponds to 19.9% of all the e-waste generated [62]. Large household
- 10 equipment, such as washing machines and refrigerators, represent around 45% of the generated and
- 11 collected e-waste [61]–[63]. Although the annual collection rate is increasing in Europe, efforts are still
  - 12 required to meet the target of 65% by the end of 2019 [64]
  - 13 For the baseline, a global average collection rate for WM of 19.9% is taken into account and the effect of
  - 14 increased collection rates is included in the scenario analysis.

#### 15 Recycling efficiencies

- Most collected e-waste is treated in a dedicated recycling plant. The treatment starts with size reduction to liberate the different material fractions. The ferrous fraction is removed magnetically. Other non-
- 18 ferrous metals, such as aluminium and copper, are removed with an eddy current seperator. Current
- 19 precious metal content in large household appliances, such as WMs, is too small to justify dedicated
- 20 shredding and separation. Extensive research was performed by Huisman et al. to establish the recovery
- 21 of the main fractions (ferrous, aluminium and copper). For metal dominated electronics, the efficiency of
- the ferrous recovery was found to be as high as 95%. The recovery of the non-ferrous was lower with an
- 23 estimated efficiency of 82,6% for aluminium and 78,2% for copper.
- Ruan et al. found that a traditional eddy current separator offered low separation efficiency of non-ferrous metallic particles from crushed e-waste [65]. Marra et al. found that only 40% of the aluminium present in the input e-waste could be traced to the aluminium output fractions, while more than 70% of the total copper was sent to the corresponding output fraction [66]. The different degree of separation observed is closely related to the form in which each metal is present in the input material. Aluminium is more often found as an allow or operandulated in multi-material agglemerates [66]. [67]
- found as an alloy or encapsulated in multi-material agglomerates [66], [67].
- 30 In 2015, a material flow analysis was conducted by sampling experiments at an e-waste treatment plant
- 31 in Belgium [68]. The losses were estimated by sampling the resulting output fractions after each separation
- 32 step. Based on the concentration and the output fraction mass, the separation efficiency of the magnet
- 33 for ferrous metal recovery and the eddy current for non-ferrous metal were estimated at 92.95% and
- 34 69.01% respectively.

1

#### 4.2. Product Circularity Indicator (PCI) -baseline results



2 3

#### Figure 5: Overview of material flow through the value chain of a washing machine

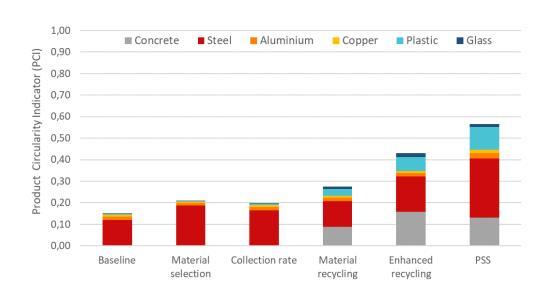
4 The collected data, as described in the previous section, are summarized in Figure 5. In total 87.72 kg of 5 input is required for the manufacture of the WM even though the product only weighs 69.51 kg. Recycled 6 feedstock represents 23% of the required input material. The metals account for most of the recycled 7 feedstock used, but they also are responsible for most of the material losses during production. Due to the 8 recyclable properties of the metals, 61% of these material losses during manufacturing are kept in the 9 material cycle as recycled scrap. Other materials, such as plastic and concrete, have a limited recycled 10 content, but generate much less production waste. Obviously, the low collection rate at end-of-life is a major loss for WMs (and other electronic products) in terms of material efficiency. In addition, only the 11 12 metals are successfully recovered from the collected WM. Consequently, on average only 38% of the 13 collected WM material is recovered. The overall calculated PCI of the WM is 0.149. Considering the PCI 14 can vary between 0 and 1, this is a rather low score. Potential improvement measures to increase the PCI 15 are discussed in the next section.

#### 16 4.3. Scenario analysis for improvement strategies based on CE thinking

Selecting more recyclable materials is sometimes assumed to increase the overall circularity performance of a product. The recyclable "material selection" scenario investigates the effect of replacing concrete with steel (cast iron) for the counterweight component. Such WMs have already been introduced on the market but are not very common due to the difference in material price between concrete and steel.

21 Increasing material recycling is an often used strategy to increase the circularity of product systems. As 22 shown in Figure 5, the overall low collection rate for electronic waste results in a significant amount of 23 unrecoverable waste. The "collection rate" scenario estimates the effect of current ambitioned European 24 collection rates. The "material recycling" scenario investigates the effect of increasing the recycling of 25 plastic, glass and concrete material. However, there are technical limitations to the potential improvement 26 of plastic recycling. First, some plastic types, such as fibre reinforced plastic (FRP), are considered 27 unrecyclable. While others, such as Polymethyl methacrylate (PMMA), are present in such low 28 concentration that separating them during waste treatment at end-of-use is not practically feasible. Both 29 recycled content of the input material ( $F_r = 0.5$ ) and recovery at end-of-use ( $E_{ms} = 0.65$  and  $E_{rfp} = 0.9$ ) are considered. Finally, the "enhanced recycling" scenario combines the increased collection rate and
 material recycling.

3 Product System Services (PSS) are often referred to as a promising CE strategy. Such a strategy can only be 4 viable if the product is well-managed at the end-of-use and increased collection rates are assumed to be 5 a consequence of the business model choice. The supplier does not sell the WM but only the service of 6 using the WM which means there is no transfer of ownership. Next to the improved collection and waste 7 management, such a business model could also increase the useful lifetime of the WM parts by introducing 8 regular maintenance and refurbishment. Based on manufacturer's expectation, the "PSS" scenario 9 assumes that the WM is refurbished every 6 years and that on average parts are used 3 times. The utility 10 factor is therefore equal to 0.6 assuming the wash frequency is unchanged. To incorporate the number of uses (N = 3) in our steady-state model, the collection for parts ( $C_u$ ) and the fraction of reused parts in 11 each WM ( $F_u$ ) are calculated as follows: 12



 $C_u = F_u = 1 - \frac{1}{N} = 0.6667$  (23)

14

15

Figure 6: PCI results for scenario analysis for improvement strategies based on CE thinking

16 The PCI results, shown in Figure 6, confirm that the improvement strategies based on CE thinking improve 17 the circularity of the product. Substituting concrete for a more recyclable material can have a positive 18 effect on the circularity performance of the product (PCI = 0.208). The circularity improvement with 19 increased collection rate is limited due to the overall low recovery for the WM. While increasing the 20 material recycling of currently unrecovered materials, such as plastic, concrete and glass, increases the PCI up to 0.276, the results of combined efforts are significantly improved (PCI=0.430). Although the current 21 22 envisioned PSS by the WM manufacturer results in a clear PCI increase (PCI=0.566), it can achieve a higher 23 circularity score by combining it with improved recycling or increasing the durability of the WM and its' 24 parts (X≥1).

### 1 4.4. Potential trade-offs with environmental performance

2 In this section, the potential trade-off between increasing circularity and minimising the environmental 3 burden of the WM is investigated. The environmental performance of the different scenario's from 4 previous section is quantified in a comparative, attributional life cycle assessment (LCA) approach, using 5 the Ecoinvent 3.3 database and the ReCiPe (H/A) endpoint method with European dataset. Although the 6 ReCiPe method has been updated in 2016, the normalisation and weighting, which allows to aggregate 7 the results in a single score, has not yet been finalized. System expansion (ISO 14040:2006) is used to 8 assure comparability of different scenarios, hence all providing the same 'basket of products'. The 9 functional unit used for this analysis is defined as the use of one WM for clothes washing, with a lifetime 10 expectancy of 2500 wash cycles.

11 The environmental impact assessment includes the following stages: (1) material production, (2) product 12 manufacturing, (3) waste management and (4) recycling. The material production is related to the amount 13 of virgin material that needs to be extracted and refined. The product manufacturing includes both the 14 production of feedstock and the final component fabrication. The material losses during manufacturing 15 are taken into account and have been quantified in previous section. The assembly phase is not 16 significantly altered in the different scenario's because it will always take place with both new and reused 17 components. For the use phase, an energy consumption in real-life conditions of 0.672 kWh/wash cycle is 18 assumed [69]. The waste management handles waste from uncollected products, production waste and 19 unrecycled rest fraction after material separation. The uncollected products at end-of-life are assumed to 20 landfilled while the production and unrecycled waste are assumed to be incinerated. The collected 21 products are assumed the be shredded followed by magnetic and eddy current separation. The metal 22 fractions are further refined to produced recycled material that can serve for new feedstock production.

Figure 7 (a) shows the LCA results for the baseline and different improvement strategies based on CEthinking. Due to the high energy consumption during each wash cycle, the use phase is identified as the life stage with the highest environmental burden. This identifies the first potential trade-off when dealing with energy-using product because the circularity measure does not take into account the burden of energy requirement during the use phase. A second trade-off identified, is the fact that selecting more recyclable material, such as steel vs. concrete, can potentially increase the overall burden.

Figure 7 (b) shows the LCA results without the dominating use phase and includes the environmental impact of the virgin material extraction for each material. The PWBs have a significant contribution in terms of environmental burden which is completely overlooked when focussing on the circularity of material streams. Nevertheless, the LCA results confirm the envisioned PSS strategy will both increase the circularity and reduce the environmental burden of the product system if the WM can indeed be successfully refurbished every 6 year and the majority of the components can be reused 3 times.

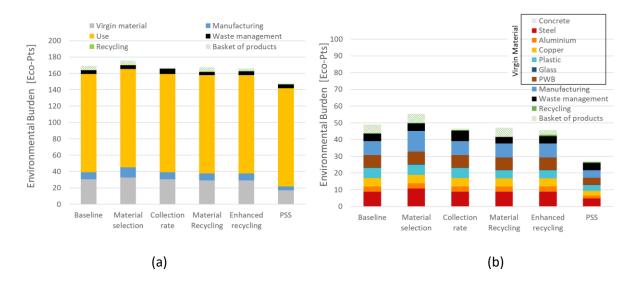


Figure 7: LCA results for scenario analysis for improvement strategies based on CE thinking (a) including the use phase (b) excluding the use and indicating the contribution of each raw material extraction

# 5. Conclusion

1

- 2 This paper researches the possibility to measure the performance of more circular complex product supply 3 chains. Although there are already a number of circularity indicators proposed in literature, none was 4 found to properly describe the product system. The Material Circularity Indicator (MCI), proposed by the 5 EMF and GD, is one of the most cited metrics at product-level. However, the indicator is unable to account 6 for the 'tightness' of the material cycles and ignores the relationship with other product system for 7 example for the use or supply of recycled material. In addition, the indicator does not take into account 8 material losses during manufacturing. Therefore, a new Product Circularity Indicator (PCI) is developed in 9 this paper and applied in a case study.
- Although the indicator is defined at product-level, a part of the dataset is collected at larger scale. For example the material production is not specific to WMs, so the average manufacturing data for semifabricated products are assumed to be representative for our case study. Unless a specific take-back scheme is put in place, the product manufacturers also have limited influence on the collected rate and end-of-life management of discarded products, and thus the use of collection data at country or regional
- 15 level are relevant.

The case study results show that the proposed PCI is a useful indicator to investigate the effectiveness of different CE strategies such as reuse of component in a Product Service Systems (PSS). The PCI can also quantify the benefits in terms of material efficiency of increased recycling, although to be effective the product should both use and supply recycled material. Finally, the PCI results demonstrate the importance of combining complementary CE strategies at different stages of the product cycle.

21 Nevertheless, there are some limitation to the proposed indicators that need to be taken into account and 22 could form the subject of future work. Currently, the different quality of recycled materials is not taken 23 into account due to the lack of an appropriate quality factor that measures quality degradation for 24 different material types. In absence of such a measure, the material value or price could be used a proxy. 25 In addition, such a weighting based on value could also be applied to the different materials included in 26 the product. In that case, more importance would be given to precious metals often present at low 27 concentration. The mining or material extraction stage is currently not included in the product system. 28 Although manufacturer and designer can choose a specific material, the origin of it is very difficult to trace 29 back. However, as ore concentration are expected to decline and new deposits become more scarce, it 30 could be useful to include this stage in future. Finally, it is important to stress the indicator only measures 31 the circularity of the flows. Other effects on the environment, typically assessed with a Life Cycle 32 Assessment, LCA, are not covered. Potential trade-offs between increasing circularity and minimizing 33 environmental burden should not be ignored.

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