

Multivariate dependent interval finite element analysis via convex hull pair constructions and the Extended Transformation Method

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Abstract

Classical (independent) interval analysis considers a hyper-cubic input space consisting of independent intervals. This stems from the inability of intervals to model dependence and results in a serious over-conservatism when no physical guarantee of independence of these parameters exists. In a spatial context, dependence of one model parameter over the model domain is usually modelled using a series expansion over a set of basis functions that interpolate a set of globally defined intervals to local (coupled) uncertainty. However, the application of basis functions is not always appropriate to model dependence, especially when such dependence does not have a spatial nature but is rather scalar. This paper therefore presents a flexible approach for the modelling of dependent intervals that is also applicable to multivariate problems. Specifically, it is proposed to construct the dependence structure in a similar approach to copula pair constructions, yielding a limited set of 2-dimensional dependence functions. Furthermore, the well-known Transformation Method is extended to the case of dependent interval analysis. The applied case studies indicate the flexibility and performance of the method.

Keywords: Interval analysis, Dependent intervals, Copula pair Constructions, non-probabilistic analysis, Transformation method, imprecise probability

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1. Introduction

Interval analysis is becoming more popular for the analysis of numerical models in case the analyst only has incomplete or vague information concerning the true parameter values, as they prove to give a more objective estimate of the uncertainty compared to probabilistic methods when insufficient data are available[1, 2]. The interval approach bounds the uncertainty concerning a model quantity by a crisp lower and upper bound. Based on these bounds, the worst-case behaviour of the structure is inferred using interval computation techniques (see e.g., [1] for a recent treatment).

Underlying these interval computations, a system of sets of partial differential equations (PDE) needs to be solved repeatedly. The approximative solution of these PDE's is usually provided by means of a numerical model $\mathcal{M}(\mathbf{x})$, parametrized by a parameter vector $\mathbf{x}(\mathbf{r}) \in \mathcal{X} \subset \mathbb{R}^{d_i}$ with \mathcal{X} the set of physically admissible parameters and $d_i \in \mathbb{N}$. For example, $\mathbf{x}(\mathbf{r})$ may contain inertial moments, clamping stiffness values or constitutive material parameters as a function of a spatial coordinate $\mathbf{r} \in \Omega \subset \mathbb{R}^{d_\Omega}$ over the model domain Ω with dimension $d_\Omega \in \mathbb{N}$, $d_\Omega \leq 4$. In case $\mathcal{M}(\mathbf{x})$ is constructed following a finite element approach, Ω is discretised by means of a set of finite elements, yielding d_d structural degrees of freedom (DOF). The model $\mathcal{M}(\mathbf{x})$ provides a vector of model responses $\mathbf{y}(\mathbf{r}) \in \mathcal{Y} \subset \mathbb{R}^{d_o}$, with \mathcal{Y} the set of admissible model responses and $d_o \in \mathbb{N}$, through a set of function operators m_i , $i = 1, \dots, d_o$, which are defined as:

$$\mathcal{M}(\mathbf{x}) : y_i(\mathbf{r}) = m_i(\mathbf{x}(\mathbf{r})) \quad i = 1, \dots, d_o \quad (1)$$

with $m_i : \mathbb{R}^{d_i} \mapsto \mathbb{R}$ Note that the dependence of \mathbf{y} on \mathbf{r} is only valid when nodal or elemental responses are considered. This is for example not the case when \mathbf{y} consists of eigenfrequencies.

One of the key challenges in the application of interval theoretical approaches for modelling uncertainty in finite element models, is the inability of intervals to account for dependence between multiple uncertain parameters. A large body of literature is therefore dedicated to minimize the over-estimation of interval

models due to this independence, following an element-by-element approach [3] or following affine arithmetic [4]. However, in some cases also dependence between multiple $x_i(\mathbf{r})$, $i = 1, \dots, d_i$ (inter-uncertainty) or $\mathbf{x}(r_i)$, $i = 1, \dots, d_\Omega$ (intra-uncertainty) has to be considered to allow for the realistic modelling of the non-deterministic structure of the model parameters. In the context of spatial dependence of a single parameter, recent work of the authors focussed on modelling spatial dependence via interval fields [5]. Following the method presented in [5], an interval field $\mathbf{x}^I(\mathbf{r}) : \Omega \times \mathbb{IR}^{n_b} \mapsto \mathbb{IR}$ is modelled as a series expansion, where local uncertainty is modelled using $n_b \in \mathbb{N}$ globally defined independent interval scalars $\alpha^I \in \mathbb{IR}^{n_b}$ and basis functions $\psi(\mathbf{r}) : \Omega \mapsto \mathbb{R}$:

$$\mathbf{x}^I(\mathbf{r}) = \sum_{i=1}^{n_b} \psi(\mathbf{r}) \cdot \alpha_i^I \quad (2)$$

13 with \mathbb{IR}^{n_b} the domain of real-valued interval vectors of dimension n_b . This
 14 framework for the modelling of spatial uncertainty modelling was recently ap-
 15 plied in the context of inverse uncertainty quantification [6, 7] and the modelling
 16 of various dynamic phenomena [8, 9, 10], as well as additively manufactured
 17 plastic components [11]. Also alternative formulations for modelling spatial
 18 uncertainty in an interval context have been proposed by other authors [12, 13].

19 However, while being valuable in the context of modelling spatial phenom-
 20 ena, when considering the dependence between multiple physical parameters
 21 of a numerical model, such a weighting approach might not be appropriate.
 22 For instance, considering parameters such as material strength and stiffness of
 23 a component that is produced using a casting approach, typically a positive
 24 dependence between such parameters would be expected. Conversely, when
 25 looking at the width and thickness of such a part, a negative dependence could
 26 be introduced due to gravitational effects. This very simple example illustrates
 27 the often highly complex nature of the combination of different dependence
 28 structures throughout a numerical model, especially when a higher-level depen-
 29 dence between strength/stiffness and width/thickness exists. Hence, a simple
 30 weighting of interval scalars using a single set of basis functions might in that
 31 case prove to be too inflexible to allow for the accurate and realistic modelling

32 of this dependence.

33 An alternative approach in this context is based on the the set-theoretical
34 work of Elishakoff and co-workers, who throughout recent years introduced sev-
35 eral set-theoretical approaches to cope with dependence in a non-probabilistic
36 way [14, 15, 16, 17]. Following the most basic approach, the dependence can be
37 represented using a d -dimensional hyper-ellipsoid which should abide by some
38 minimum volume property. Also extensions towards Lamé curves and other,
39 nodal, convex sets were introduced in recent years [18, 19]. However, while pro-
40 viding the analyst with an intuitive tool, the underlying assumption is still that
41 all parameters are governed by a single underlying dependence structure. A so-
42 lution hereto could be to only consider pair-wise dependence, but this neglects
43 possible higher-order dependence structures between multiple model quantities.

44 In the context of probabilistic modelling of uncertainty, techniques based on
45 Copula [20] are being applied widely, for instance in the modelling of dependence
46 in system reliability [21], naval engineering [22] or inverse Bayesian random field
47 quantification [23]. Application of these methods extend also far beyond the
48 engineering realm with for example wide application in financial mathematics
49 [24] and machine learning [25]. These methods indeed provide a flexible tool
50 to model complex dependencies in an intuitive and elegant way, but sampling
51 from a copula in $d > 2$ proves to be a daunting task [21]. Furthermore, also here
52 the argumentation holds that it is questionable to model all dependency using a
53 single Copula family (i.e., dependence structure). As a possible solution hereto,
54 Copula pair constructions were introduced in the seminal papers of Bedford
55 and Cooke [26, 27] and further elaborated on by Aas [28]. The core idea hereof
56 is to decompose the multivariate, higher-order dependencies as a product of
57 marginal distributions, a set of 2-dimensional unconditional Copula and a set
58 of conditional Copula, allowing for the definition of a dependence structure for
59 each combination of parameters. However, these methods rely heavily on the
60 underlying statistical derivations and hence, it is unclear how these methods
61 should be applied in an interval context without violating the interval paradigm
62 where only crisp bounds on the uncertain quantities are considered.

63 This paper therefore explores the application of copula pair construction
64 approaches for the modelling of dependence between uncertain parameters of a
65 FE model that are modelled as intervals. Specifically, it is aimed at introducing
66 a generic set-theoretical method that allows an analyst to define a high-order
67 dependence structure as a product of 2-dimensional, possibly non-convex, ad-
68 missible sets that bound the combination of parameter values within \mathbf{x}^I . Hereto,
69 the bounded global optimisation problem that underlies typical interval com-
70 putations is recast into a non-linear constrained global optimisation problem
71 to accommodate these higher-order dependence structures. The paper is struc-
72 tured as follows. In section 2, a concise introduction to copula in a probabilistic
73 context is presented. Then, section 3 proposes a new set-theoretical method to
74 propagate multivariate interval uncertainty with dependence between the inter-
75 val valued parameters. Section 5 and 6 present two case studies to illustrate the
76 application of these ideas to both an academic case study as well as a realistic
77 finite element model. Conclusions are listed in section 7.

78 2. Copula in a probabilistic context

79 This section introduces Copula and Copula pair constructions in a concise
80 way. It is not intended to provide the reader with a mathematically thorough
81 introduction to Copula since this lies outside the scope of this paper, but rather
82 to convey the general ideas that are needed in the development of the new
83 interval method.

84 2.1. Copula

A Copula C is a function that constructs a joint cumulative distribution
function $F_{1:d_i}(x_1, x_2, \dots, x_{d_i})$, with $x_1, x_2, \dots, x_{d_i} \in [0, 1]^{d_i}$ starting from its one-
dimensional marginal distribution functions F_i , $i = 1, \dots, d_i$. As such, the mod-
elling of the dependence is decoupled from the modelling of the non-determinism
in the model parameters via their marginals. The application of Copula on a
bivariate distribution is based on Sklar's theorem [20]:

$$F_{1:d_i} = C_{1:d_i}(F_1(x_1), F_2(x_2), \dots, F_{d_i}(x_{d_i})) \quad (3)$$

$\forall \mathbf{x} \in \mathbb{R}^{d_i}$, with $C_{1:d_i} : [0, 1]^{d_i} \mapsto [0, 1]$ the copula function. In case all F_i , $i = 1, \dots, d_i$ are continuous, $F_{1:d_i}$ is unique. Note that a copula is always contained between the Fréchet-Hoeffding bounds:

$$\max \left(1 - d_i + \sum_{i=1}^{d_i} x_i, 0 \right) \leq C_{1:d_i} \leq \min(x_i) \quad (4)$$

85 which bound the dependence between the parameters and correspond to the
 86 probability mass lying on the principal diagonals of $[0, 1]^{d_i}$.

Two types of families are directly applicable to cases where $d_i > 2$: Gaussian and Archimedean copula, and hence, attract a lot of scientific and industrial interest. The Gaussian copula is defined as:

$$F_{G,1:d_i} = \Phi_{d_i}(\Phi^{-1}(u_1), \dots, \Phi^{-1}(u_{d_i})) \quad (5)$$

87 with $u_i \in [0, 1]$ a coordinate in standard normal space, $\Phi^{-1}(u_i) \mapsto$ the inverse
 88 univariate cumulative distribution function of u_i and $\Phi_{d_i} \mapsto$ the cumulative
 89 distribution function as $\mathcal{N}(0, R)$ and $R \in \mathbb{R}^{d_i \times d_i}$ a positive definite correlation
 90 matrix. As such, this corresponds to the well-known Nataf function. The defi-
 91 nition of Archimedean copula is similar as in eq. (5), with the main difference
 92 being that $\Phi^{-1}(u_i)$ and Φ_{d_i} are replaced by a so-called generator function and
 93 its inverse [29]. The formulation of the generator function depends on the copula
 94 family (e.g., Frank, Gumbel, Planck and so forth). However, it may not be
 95 physically accurate to use the same copula family (i.e., dependence structure)
 96 to model the dependence between all combinations of parameters since this de-
 97 pendence is in general not the same. Furthermore, sampling from a copula in
 98 $d > 2$ proves to be a daunting task [21].

99 2.2. Pair Copula Construction

100 To overcome the limitations of these *regular* copula, the d_i -dimensional den-
 101 sity $f(x_1, \dots, x_{d_i})$ of a random vector $\mathbf{X} = (X_1, X_2, \dots, X_n)$ is constructed
 102 using a product of $d(d-1)/2$ bivariate (conditional) copula [26, 28].

As a first step, expressing eq. (3) for continuous, strictly monotonic marginal density functions f_1, \dots, f_n via derivation w.r.t. x yields:

$$f(x_1, \dots, x_{d_i}) = c_{1, \dots, d_i}(f_1(x_1), \dots, f_n(x_n)) \cdot f_1(x_1) \cdots f_{d_i}(x_{d_i}) \quad (6)$$

where c_{1, \dots, d_i} is a uniquely defined d_i -dimensional copula density function. The copula-pair construction is based on following factorisation of $f(x_1, \dots, x_{d_i})$:

$$f(x_1, \dots, x_{d_i}) = f_{d_i}(x_{d_i}) \cdot f(x_{d_i-1} | x_{d_i}) \cdot f(x_{d_i-2} | x_{d_i-1}, x_{d_i}) \cdots f(x_1 | x_2, \dots, x_{d_i}) \quad (7)$$

which is a product of conditional and unconditional marginals. Taking into account eq. (6), each term in eq. (7) can be decomposed as:

$$f(x | \mathbf{v}) = c_{xv_j | \mathbf{v}_{-j}}(F(x | \mathbf{v}_{-j}) | F(v_j | \mathbf{v}_{-j})) \cdot f(x | \mathbf{v}_{-j}) \quad (8)$$

103 for a general vector \mathbf{v} [28].

104 Hence, the factorisation given in eq. (7) can be constructed as a product
 105 of $d(d-1)/2$ bivariate (conditional) copula and their marginals [26, 28]. This
 106 enables the modelling of dependence between two x_i with a much higher degree
 107 of flexibility, since different c_{ij} can be employed for all x_i .

108 For instance, when considering a three-dimensional random vector $\mathbf{X} =$
 109 (X_1, X_2, X_3) and applying eq. (8), the bivariate densities can be written as:

$$f_{2|1}(x_2|x_1) = c_{12}(f_1(x_1), f_2(x_2)) \quad (9)$$

$$f_{3|2}(x_3|x_2) = c_{32}(f_3(x_3), f_2(x_2)) \quad (10)$$

$$f_{3|12}(x_3|x_1, x_2) = c_{13|2}(f_{1|2}(x_1|x_2), f_{3|2}(x_3|x_2)) \quad (11)$$

which yields:

$$f(x_1, x_2, x_3) = f_1(x_1) \cdot f_2(x_2) \cdot f_3(x_3) \cdot c_{12}(f_1(x_1), f_2(x_2)) \cdot c_{23}(f_2(x_2), f_3(x_3)) \cdot c_{13|2}(f_{1|2}(x_1|x_2), f_{3|2}(x_3|x_2)) \quad (12)$$

with $c_{ij|k}$ the bivariate copula linking F_i and F_j conditional on x_k . For higher d_i , a similar construction can be made. As can be noted, a large number of constructions can be contrived when d_i is large. Most commonly, therefore a set

of nested trees is used to visualise and enumerate these constructions via graph theory. Such set of nested trees is also referred to as a "vine copula". Following a \mathfrak{D} -vine decomposition, the copula can be constructed as:

$$f_{1,\dots,d_i}(x_1, x_2, \dots, x_{d_i}) = \prod_{k=1}^{d_i} f(x_k) \prod_{j=1}^{d_i-1} \prod_{i=1}^{d_i-j} c_{i,i+j|i+1,\dots,i+j+1} \quad (13)$$

$$(F(x_i|x_{i+1}, \dots, x_{i+j-1}), F(x_{i+j}|x_{i+1}, \dots, x_{i+j-1}))$$

Alternatively, the d_i -dimensional copula can also be represented following a \mathfrak{C} -vine decomposition:

$$f_{1,\dots,d_i}(x_1, x_2, \dots, x_{d_i}) = \prod_{k=1}^{d_i} f(x_k) \prod_{j=1}^{d_i-1} \prod_{i=1}^{d_i-j} \mathcal{D}_{j,j+i|1,\dots,j-1} \quad (14)$$

$$(F(x_j|x_{j=1}, \dots, x_{j+1}), F(x_{j+i}|x_1, \dots, x_{j-1}))$$

110 An extensive literature exists discussing many aspects of Copulas, Copula
 111 pair constructions and different types of vine copula. The interested reader is
 112 referred to [28] or the book of Mai and Scherer [29].

113 3. A copula based approach for interval finite element computations

114 3.1. Interval finite element method

The goal of an interval FE calculation is to find the bounds on the uncertainty in the model responses of eq. (1), given an interval description of the uncertainty in $\mathbf{x}^I \in \mathcal{X}^I \subset \mathbb{I}\mathbb{R}^{d_i}$. For multiple parameters, the interval vector \mathbf{x}^I is defined as the Cartesian product of the intervals x_i^I :

$$\mathbf{x}^I = x_1^I \times \dots \times x_{d_i}^I \quad (15)$$

and as such spans a hypercubic set by definition [1]. The interval FE method can as such be expressed as finding the solution set $\tilde{\mathbf{y}}$:

$$\tilde{\mathbf{y}} = \{\mathbf{y} | \mathbf{y} = \mathcal{M}(\mathbf{x}); \mathbf{x} \in \mathbf{x}^I\} \quad (16)$$

Generally, $\tilde{\mathbf{y}}$ spans a non-convex manifold in \mathbb{R}^{d_o} , as the output responses y_i are (possibly non-linearly) coupled through the PDE of the FE model under consideration. Therefore, instead of calculating the *real* uncertain solution

set spanned by $\tilde{\mathbf{y}}$, the uncertainty at the output of the FE model generally is approximated using an interval vector \mathbf{y}^I , which is usually calculated following a bounded optimisation problem, where the bounds \underline{y}_i and \bar{y}_i on each output quantity y_i of the solution interval vector \mathbf{y}^I are determined by searching the domain, defined by \mathbf{x}^I [1]:

$$\begin{aligned} \underline{y}_i &= \min_{\mathbf{x} \in \mathbf{x}^I} m_i(\mathbf{x}) & i = 1, \dots, d_o \\ \bar{y}_i &= \max_{\mathbf{x} \in \mathbf{x}^I} m_i(\mathbf{x}) & i = 1, \dots, d_o \end{aligned} \tag{17}$$

115 where $y_i^I = [\underline{y}_i; \bar{y}_i]$ is the result interval scalar for the i^{th} component of the
 116 solution interval vector of the model. This optimization problem has been shown
 117 to be solved with both local and global optimization algorithms [1]. Solution
 118 of equation (17) returns the smallest hyper-cubic approximation \mathbf{y}^I of $\tilde{\mathbf{y}}$. Also
 119 methods that try to estimate $\tilde{\mathbf{y}}$ by its smallest convex set, [30], or based on
 120 affine arithmetic, have been proposed in recent years [31]. Also convex hulls
 121 have been applied in this context [6, 7, 32].

122 3.2. Bivariate dependence between intervals

123 In a bivariate context, the concept of dependence can be illustrated using
 124 figure 1. This figure shows two arbitrary parameters x_1 and x_2 . The correspond-
 125 ing uncertainty is scaled for both parameters to the interval $[0,1]$ for illustrative
 126 purposes, which is a straightforward operation on the data. In case no depen-
 127 dence between these parameters is taken into account, the space of admissible
 128 parameter combinations corresponds to the unit square $[0, 1]^2$, which is also il-
 129 lustrated using the striped line. However, in case dependence is present between
 130 these two parameters, this can be modelled in an interval context by defining
 131 a set \mathcal{D}_{12} that limits the range of admissible parameter combinations. This set
 132 is denoted the admissible set, and as such, the analysis becomes more generally
 133 set-theoretical (as intervals are a very specific type of convex sets). The degree
 134 of dependence can then be computed as the relative area of \mathcal{D}_{12} with respect to
 135 $[0, 1]^2$ [33].

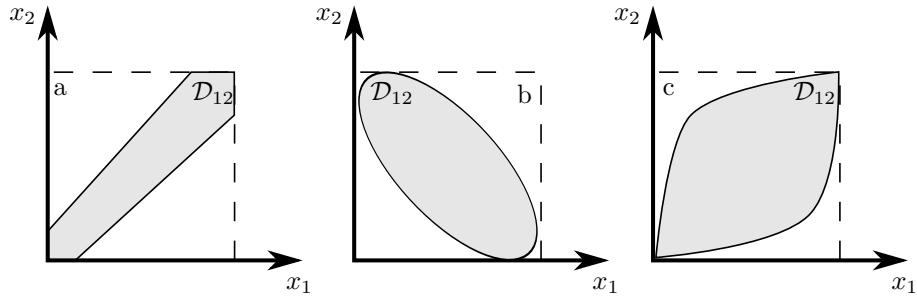


Figure 1: Illustration of dependence between two arbitrary parameters x_1 and x_2 , modelled as a convex region \mathcal{D}_{12} .

136 The definition of \mathcal{D}_{12} can be based on expert knowledge, first principle fun-
 137 damentals, joint measurements of the uncertain parameters, etc. and \mathcal{D}_{12} can
 138 take any shape within $[0, 1]^2$, as long as it is physically relevant. For example,
 139 in an interval context, an admissible set that resembles the well-known diagonal
 140 band copula [34] can be applied as it requires only one additional parameter
 141 to be defined next to the interval uncertainty. In the specific case of figure 1,
 142 in figure 1 a) a dependence is assumed that slightly decreases as x_1 and x_2
 143 increase, figure 1 b) illustrates a negative ellipse-shaped dependence, as is for
 144 instance commonly applied in convex analysis [17]. Finally figure 1 c) illustrates
 145 a large dependence in the centre of $[0, 1]^2$ and small dependence around the ex-
 146 treme values of the interval. Evidently, this illustration of admissible sets is not
 147 exhaustive.

In the context of propagating this set-theoretical uncertainty, the optimiza-
 tion problem that is introduced in eq. (17) becomes a constrained optimization
 problem:

$$\begin{aligned} \underline{y}_i &= \min_{\mathbf{x} \in \mathbf{I}} m_i(\mathbf{x}) & i = 1, \dots, d_o \\ \text{s.t. } & \mathbf{x} \in \mathcal{D}_{12} \end{aligned} \tag{18}$$

148 In case \mathcal{D}_{12} is a convex nodal set (i.e., a set that is defined by half-spaces),
 149 this reduces to a linearly inequality constrained optimization problem. In other
 150 cases, such as for instance an ellipsoidal admissible set, this becomes a non-linear
 151 constraint. If the underlying numerical model is sufficiently smooth, Newton-

152 type optimizers can be applied to solve this problem as they are highly efficient
 153 [35]. In other cases, when the model is for instance highly non-linear or bi-
 154 furcated, semi-heuristic optimization algorithms such as Genetic optimizers or
 155 Particle Swarm algorithms have to be applied, which are in general less efficient.
 156 Application of both types of optimizers has been documented in the context of
 157 the propagation of interval algorithms [1, 36].

158 In case more than 3 parameters are considered, the definition of \mathcal{D} might
 159 prove to be very cumbersome or even impossible, since this requires the def-
 160 inition of a $d_i > 3$ dimensional convex set, which is intuitively speaking an
 161 impossible task. Therefore, a decomposition of the admissible set, based on the
 162 concept of copula pair construction is introduced in the next section.

163 3.3. Admissible set decomposition

164 In order to allow for a more flexible modelling of the joint-dependence struc-
 165 ture of the interval uncertainty, captured by its admissible set, a similar pair
 166 construction as shown in eq. (7) and (12) is presented. Intuitively and loosely
 167 speaking, it can be argued that an admissible set \mathcal{D} is some kind of piece-wise
 168 continuous copula, however without inferring any likelihood of certain param-
 169 eter values within \mathcal{D} . The premise of this section is therefore that \mathcal{D} can be
 170 similarly decomposed in the product of bivariate (conditional) \mathcal{D}_{ij} and their
 171 marginal intervals.

172 However, the definitions of \mathcal{D} and \mathcal{C} -vine copula, as presented respectively
 173 in eq. (13) and (14) cannot be translated directly to an interval context. A
 174 direct and naive translation would involve changing the random variables by
 175 intervals and the copula densities by bivariate admissible sets. This however is
 176 not advisable since intervals cannot track dependence throughout computations,
 177 and hence, this would inflate the interval bounds dramatically (see e.g., [1]
 178 for a discussion on this phenomenon). Instead, it is proposed to recast the
 179 decomposition into a product of inequality constraints bounding the search space
 180 of the optimization problem introduced in (17) from \mathbf{x}^I to \mathcal{D} .

Specifically, it is proposed to formulate the \mathfrak{D} -vine decomposition of the

admissible set $\mathcal{D}_{1,\dots,d_i}(x_1^I, x_2^I, \dots, x_{d_i}^I)$ as:

$$\mathcal{D}_{1,\dots,d_i}(x_1^I, x_2^I, \dots, x_{d_i}^I) = \bigotimes_{k=1}^{d_i} x_k^I \bigcap_{j=1}^{d_i-1} \bigcap_{i=1}^{d_i-j} \mathcal{D}_{i,i+j|i+1,\dots,i+j+1} \quad (19)$$

181 where the operator \bigotimes is used to denote the Cartesian product of the inter-
 182 vals, and hence, the first part of the equation just describes the d_i dimensional
 183 hyper-cube of independent intervals. The dependence is included by computing
 184 intersections of this hyper-cubic space with (conditional) bivariate admissible
 185 sets that are defined in analogy with the conditional bivariate copula densities
 186 in a probabilistic (vine-copula) approach. The \mathfrak{D} -vine decomposition is advan-
 187 tageous when the dependence structure of the admissible set is governed mostly
 188 by certain sets of piecewise-dependent parameter combinations. In that case,
 189 those can be modelled explicitly, whereas the higher order interactions between
 190 those parameters are separated.

Similarly, a \mathfrak{C} -vine decomposition is expressed as:

$$\mathcal{D}_{1,\dots,d_i}(x_1^I, x_2^I, \dots, x_{d_i}^I) = \bigotimes_{k=1}^{d_i} x_k^I \bigcap_{j=1}^{d_i-1} \bigcap_{i=1}^{d_i-j} \mathcal{D}_{j,j+i|1,\dots,j-1} \quad (20)$$

191 which is advantageous when the dependence of one parameter with all other
 192 parameters is rather easy to quantify [37]. In that case, the lower-order de-
 193 pendence structure of the admissible set can be build completely around this
 194 central parameter.

195 As such, the admissible domain inside \mathbf{x}^I can be fully described by a set of
 196 bivariate \mathcal{D}_{ij} . Since the definition of a two-dimensional admissible set is much
 197 more intuitive from an analysts point of view, this is easier as compared to defin-
 198 ing the full d_i -dimensional \mathcal{D} . Furthermore, since the higher-order, conditional
 199 $\mathcal{D}_{ij|k}$ can be made a function of x_k , this allows for the highly flexible modelling
 200 of complex dependence structures in an interval context.

For a three-dimensional interval vector $\mathbf{x}^I = [x_1^I, x_2^I, x_3^I]$, the \mathfrak{D} -vine repre-
 sentation reduces to:

$$\mathcal{D}(x_1^I, x_2^I, x_3^I) = x_1^I \times x_2^I \times x_3^I \cap \mathcal{D}_{12} \cap \mathcal{D}_{23} \cap \mathcal{D}_{13|2} \quad (21)$$

201 with \mathcal{D}_{ij} the bivariate dependence between x_i and x_j . This concept is also
 202 illustrated in figure 2. This figure shows the unit cube $[0, 1]^3$, together with
 203 \mathcal{D}_{12} , \mathcal{D}_{23} and $\mathcal{D}_{13|2}$. As can be noted, the set $\mathcal{D}_{13|2}$ is not necessarily constant
 204 over x_2 , allowing for the definition of highly complicated dependence structures
 with a very limited set of parameters.

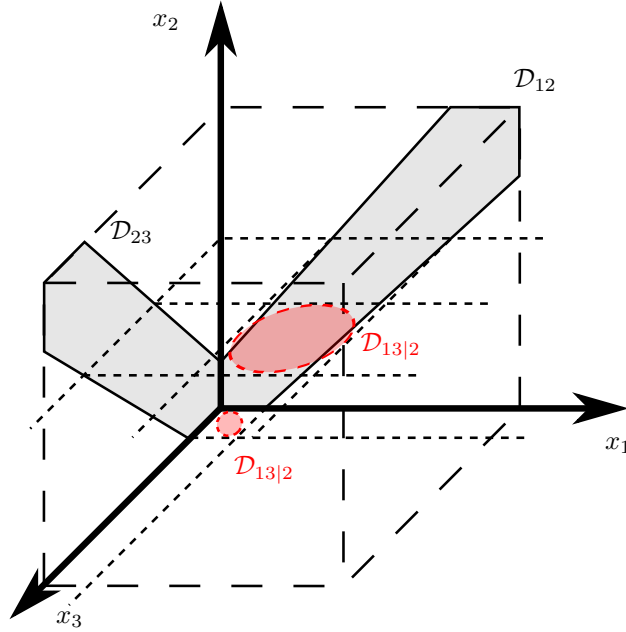


Figure 2: Decomposition of the $d = 3$ -dimensional dependence using the proposed admissible set decomposition via a \mathfrak{D} -vine structure.

205

Similarly, for a three-dimensional interval vector $\mathbf{x}^I = [x_1^I, x_2^I, x_3^I]$, the \mathfrak{C} -vine representation reduces to:

$$\mathcal{D}(x_1^I, x_2^I, x_3^I) = x_1^I \times x_2^I \times x_3^I \cap \mathcal{D}_{12} \cap \mathcal{D}_{13} \cap \mathcal{D}_{23|1} \quad (22)$$

206 with \mathcal{D}_{ij} the bivariate dependence between x_i and x_j . Note that for a three-
 207 dimensional case, both \mathfrak{D} - and \mathfrak{C} -vine structures give the same decomposition.
 208 Both representations allow to decouple any information that an analyst has on
 209 the dependence between combinations of interval-valued parameters from the
 210 actual magnitude of the uncertainty, and hence, are also in an interval context

211 a very powerful tool.

212 Note that, while employing a similar decomposition structure as in a prob-
213 abilistic context, the underlying meaning is fundamentally different. Instead of
214 decomposing a multivariate density function, into its marginals and a set of bi-
215 variate copula, this method presents a way to limit the hypercube $x_1^I \times \dots \times x_d^I$
216 of admissible values by a set of two-dimensional sets. While similar, still no
217 inference of the likelihood of certain values within this set is made or aimed at.
218 As such, the interval paradigm is not violated following this approach. Further-
219 more, the presented method can be regarded as a generalization of the work on
220 dependence between non-probabilistic quantities presented in e.g., [5] or [14].
221 For instance, when all bi-variate admissible sets are considered ellipsoidal, one
222 would end up with a high-dimensional ellipsoid.

223 The presented method is especially of practical interest in case an analyst
224 has quantified information about bivariate dependence between two quantities
225 in the model. For instance, consider the case of additively manufactured com-
226 ponents. In those parts, underlying physical process parameters jointly affect
227 mechanical quantities such as strength and stiffness, but also dimensional quan-
228 tities such as the part thickness (see e.g., [38]). Instead of trying to quantify
229 and model the full dependence structure of all these uncertain quantities at
230 once, the analyst can focus on quantifying a limited set of bivariate dependence
231 structures, and constructing the full-dimensional dependence from these. As
232 a second example of application, when an analyst is currently faced with say,
233 20 uncertain model quantities, ranging from bolt connection stiffness values to
234 localized masses and support stiffness values (as is the case in e.g., the DLR
235 AIRMOD structure [2]), (s)he either can opt to consider all parameters inde-
236 pendent and work hyper-cubic via the classical interval paradigm or assume a
237 similar dependence structure among all parameters, and employ classical con-
238 vex set approaches. Following this approach, the analyst can make e.g., directed
239 measurements of certain parameters of interest and fit a certain convex structure
240 to those (in analogy to the work presented in [18, 19]), use expert knowledge to
241 model other dependencies as ellipses, and so on. Hence, a more flexible approach

242 for the modelling of dependence is provided by considering this decomposition
 243 of \mathcal{D} in bivariate admissible sets.

244 4. Propagation of the admissible set

245 This section presents two approaches to propagate the admissible set through
 246 a numerical model. The first approach converts the well-known global optimiza-
 247 tion approach into a constraint global optimization approach that is able to
 248 account for the dependence between the model responses. The second approach
 249 extends the Transformation Method, as presented by Hanss in [30] towards the
 250 propagation of (set-theoretical) dependent intervals.

251 4.1. Global optimization

252 In the context of propagating this uncertainty through the numerical model,
 253 this decomposition serves as a constraint for the global optimization that un-
 254 derlies the interval finite element model. Specifically, to infer the bounds on y ,
 255 following set of constrained optimization problems is solved:

$$\underline{y}_i = \min_{\mathbf{x} \in \mathbf{x}^I} m_i(\mathbf{x}) \quad \text{s.t. } \mathbf{x} \in \mathcal{D}(x^I) \quad (23)$$

$$\bar{y}_i = \max_{\mathbf{x} \in \mathbf{x}^I} m_i(\mathbf{x}) \quad \text{s.t. } \mathbf{x} \in \mathcal{D}(x^I) \quad (24)$$

256 for $i = 1, \dots, d_o$, which can be solved by most Newton-type or semi-heuristic op-
 257 timization algorithms. Moreover, since the convex hulls are only 2-dimensional,
 258 the corresponding computational overhead for evaluating these equality con-
 259 straints is very limited [6].

260 4.2. The enriched transformation method

261 Alternatively, when monotonic models \mathcal{M} are considered, als a semi-analytic
 262 approach can be applied. Instead of handling the problem as a black-box, the
 263 intersections of the bivariate admissible sets with the hyper-cubic interval space
 264 are computed and the nodes of the resulting polytopes are propagated through
 265 the FE model. The necessary steps to perform these computations are described
 266 in the following section.

As a first step, the hyper-cubic input uncertainty $\mathbf{x}^I = x_1^I \times x_2^I \times x_{d_i}^I$ is represented as a set of linear inequalities:

$$\mathbf{x}^I \equiv A_{hc}x - b_{hc} \geq 0 \quad (25)$$

267 with $A_{hc} \in \mathbb{R}^{h_x \times d_i}$, $x \in \mathbb{R}^{d_i}$ and $b_{hc} \in \mathbb{R}^{h_x}$. Herein, h_x is the number of
 268 linear inequalities that are necessary to bound the admissible set. According to
 269 Minkowski-Weyl's theorem both representations are equivalent.

Then, similarly to eq. (25), each bivariate admissible set from eq. (19) or eq. (20) is represented as a set of 2-dimensional linear inequalities:

$$\mathcal{D}_{\mathcal{I}(i)} \equiv A_{\mathcal{I}(i)}x - b_{\mathcal{I}(i)} \geq 0 \quad i = 1, \dots, d_i(d_i - 1)/2 \quad (26)$$

270 with $A \in \mathbb{R}^{h_x \times 2}$, $x \in \mathbb{R}^2$ and $b_i \in \mathbb{R}^{h_x}$. $\mathcal{I}(i)$ is an index set containing the
 271 indices of the $d_i(d_i - 1)/2$ conditional and unconditional bivariate admissible
 272 sets. Each of these sets describes the dependence in a two-dimensional inter-
 273 section of the full admissible set \mathcal{D} . As such, \mathcal{D} can be obtained by asserting
 274 that admissible parameter values should satisfy the linear inequalities in each
 275 of these intersections.

In a first step, only the unconditional bivariate admissible sets are considered. Since not each $\mathcal{D}_{\mathcal{I}(i)}$ contains information on the same $x_i, i = 1, \dots, d_i$, these projections have to be assembled as follows:

$$\mathcal{D}_u \equiv A_u \mathbf{x} - b_u \geq 0 \quad (27)$$

with $A_u =$

$$\begin{bmatrix}
 a_{hc}(1, x_1) & a_{hc}(1, x_2) & \cdots & a_{hc}(1, x_{d_i-1}) & a_{hc}(1, x_{d_i}) \\
 a_{hc}(2, x_1) & a_{hc}(2, x_2) & \cdots & a_{hc}(2, x_{d_i-1}) & a_{hc}(2, x_{d_i}) \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 a_{hc}(h_s, x_1) & a_{hc}(h_s, x_2) & \cdots & a_{hc}(h_s, x_{d_i-1}) & a_{hc}(h_s, x_{d_i}) \\
 a_{\mathcal{I}(1)}(1, x_1) & a_{\mathcal{I}(1)}(1, x_2) & \cdots & 0 & 0 \\
 a_{\mathcal{I}(1)}(2, x_1) & a_{\mathcal{I}(1)}(2, x_2) & \cdots & 0 & 0 \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 a_{\mathcal{I}(1)}(h_{12}, x_1) & a_{\mathcal{I}(1)}(h_{12}, x_2) & \cdots & 0 & 0 \\
 \vdots & \vdots & \vdots & \vdots & \vdots \\
 0 & 0 & \cdots & a_{\mathcal{I}(d_i-1)}(h_{\mathcal{I}(d_i-1)}, x_{d_i-1}) & a_{\mathcal{I}(d_i-1)}(h_{\mathcal{I}(d_i-1)}, x_{d_i})
 \end{bmatrix}
 \quad (28)$$

and b_u :

$$b_{full} = \begin{bmatrix}
 b_{hc}(1) \\
 b_{hc}(2) \\
 \vdots \\
 b_{hc}(d_i) \\
 b_{\mathcal{I}(1)}(1) \\
 b_{\mathcal{I}(1)}(2) \\
 \vdots \\
 b_{\mathcal{I}(1)}(d_i) \\
 \vdots \\
 b_{\mathcal{I}(d_i-1)}(d_i)
 \end{bmatrix}
 \quad (29)$$

In case only unconditional admissible sets are defined, the space of all admissible $\mathbf{x} \in \mathcal{D}$ is fully determined. This is for instance the case when only pair-wise dependence structures need to be constructed. The final step is then to propagate all vertices of \mathcal{D} through \mathcal{M} . The realization set $\tilde{\mathbf{y}}$ is then obtained as:

$$\tilde{\mathbf{y}} = \{\mathbf{y} | \mathbf{y} = \mathcal{M}(\mathbf{x}); \mathbf{x} \in \mathcal{D}\}
 \quad (30)$$

276 where the bounds of the set are constructed using linear interpolation between

277 the propagated nodes.

When also conditional admissible sets are included in the analysis, further intersections of \mathcal{D}_u have to be computed sequentially. For instance, to compute the conditional admissible set $\mathcal{D}_{13|2}$, the parameter space is first uniformly discretized over x_2 into n bins:

$$x_2 = \{x_2^1, x_2^2, \dots, x_2^n\} \quad (31)$$

with:

$$x_2^e - x_2^1 = \frac{\bar{x}_2 - x_2^1}{n} \quad (32)$$

278 providing slices of \mathcal{D}_u for each x_2^e . Then, each of this slices is intersected with the
279 the corresponding conditional admissible set. Those slices are finally recombined
280 to reconstruct the admissible set \mathcal{D} including the conditional admissible sets.

281 It should be noted that the computational cost of the method can scale badly
282 for large scale problems and complicated dependence structures. The applica-
283 tion of the transformation method for independent intervals already requires 2^{d_i}
284 deterministic function evaluations. In case dependence is included in the anal-
285 ysis, only more vertices of the admissible set need to be propagated through
286 \mathcal{M} and hence, those calculations can become expensive. A priori estimation of
287 the increase in computational cost is highly non-trivial. Indeed, the computa-
288 tional cost is directly related to the number of vertices in \mathcal{D} , which in its turn is
289 dependent on the number of bivariate admissible sets that are included in the
290 analysis, as well as the level of their mutual dependence.

291 Application of surrogate modeling techniques such as Kriging [39, 40] or
292 Artificial Neural Networks [2, 41] have, among many other techniques (see e.g.,
293 [1] for a recent overview), already proven their merit in the context of interval
294 computations.

295 **5. Case study 1: analytical function**

As a first example, dependent interval uncertainty is propagated through a simple analytical equation having three parameters x_i , $i = 1, \dots, 3$:

$$y = x_1 \cdot x_2 - 2 \cdot x_3 \quad (33)$$

296 with $x_1^I = [1, 4]$, $x_2^I = [2, 6]$, $x_3^I = [3, 5]$.

297 This function is constructed such that the extreme values for y do not cor-
 298 respond with either \underline{x} or \bar{x} . The dependence between these parameters assumes
 299 following structure:

$$\mathcal{D}_{12} = \mathcal{H}(|x_2 + x_1 - 1| - \theta_1) \quad (34)$$

$$\mathcal{D}_{23} = \mathcal{H}(|x_1 - x_2| - \theta_2) \quad (35)$$

$$\mathcal{D}_{13|2} = \mathcal{H}(|x_3(x_2) - x_1(x_2)| - \theta_3(x_2)) \quad (36)$$

300 with \mathcal{H} the Heaviside function, θ_i a measure for the dependence and $||$ denoting
 301 the absolute value. For the construction of the admissible set \mathcal{D} the problem is
 302 first scaled to the unit cube $[0, 1]^3$. The tested values for the dependency are
 303 listed in table 1. The $\hat{\bullet}$ operator indicates the interval that yields the extreme
 304 values for y .

305 The admissible set \mathcal{D} , as illustrated in eq. (19), is constructed based on
 306 eqns. (34) - (36). The *enriched transformation method* is applied to discretise
 307 \mathcal{D} into a set of vertices, which then are used to propagate the dependent inter-
 308 vals. To construct the admissible sets that are conditional on x_2 , the domain
 309 x_2 is discretised in 100 elements. The computation of the intersections and con-
 310 version of the convex hulls into half-spaces, the Matlab FEX package *Analyse*
 311 *N-dimensional Polyhedra in terms of Vertices or (In)Equalities* was used.

312 As can be noted, the results without dependence between the interval param-
 313 eters are highly over-conservative with respect to the case when the dependence
 314 is taken into account following the proposed set-theoretical approach. The de-
 315 gree of conservatism decreases when the parameters in θ are increased, as this
 316 increases the dependence between the intervals by reducing the size of \mathcal{D} . Fur-
 317 thermore, it can be noted that the necessary number of function evaluations

318 increases with the number of bivariate admissible sets that are taken into ac-
319 count. Especially inclusion of conditional admissible sets leads to a significant
320 increase in number of function evaluations, which is due to the discretisation of
321 the conditional axis. Post-processing of the assembled admissible set, e.g., by
322 performing regression on the bounding half-spaces, could solve this issue. This
323 is however outside the scope of this paper.

Table 1: Results of the propagation of the interval uncertainty and admissible set in eq. (33)

$\theta = [\theta_1, \theta_2, \theta_3]$	\hat{x}	\hat{x}	y^I	# eval.
[0, 0, 0]	[1, 2, 5]	[4, 6, 3]	[-8, 18]	8
[0.25, 0, 0]	[1, 3, 5]	[4, 5, 3]	[-6, 14]	12
[0, 0.25, 0]	[1, 3, 5]	[4, 6, 3.5]	[-7, 17]	12
[0.25, 0.25, 0]	[1, 3, 5]	[4, 5, 3]	[-7, 14]	14
[0.25, 0.25, 0.25]	[1, 3, 4.5]	[4, 5, 3.5]	[-6, 13]	700
[0.5, 0, 0]	[1, 4, 5]	[4, 4, 3]	[-6, 10]	12
[0, 0.5, 0]	[1, 4, 5]	[4, 6, 4]	[-6, 16]	12
[0.5, 0.5, 0]	[1, 4, 5]	[4, 4, 3]	[-6, 10]	12
[0, 0, 0.5]	[1, 2, 4]	[4, 6, 4]	[-6, 16]	700
[0.5, 0.5, 0.5]	[1, 4, 4]	[3.75, 4.33, 4.08]	[-4, 8.08]	700
[0.75, 0, 0]	[1, 5, 5]	[4, 3, 3]	[-5, 6]	12
[0, 0.75, 0]	[1, 2, 3.5]	[464.5]	[-5, 15]	700
[0.75, 0.75, 0]	[1, 5, 5]	[4, 3, 3]	[-5, 6]	14
[0.75, 0.75, 0.75]	[1, 5, 4.25]	[3.625, 3.5, 4]	[-3.5, 4.687]	700

324 As was explained in section 3, the higher order dependence terms can be
325 made a function of the conditional parameter. Table 2 illustrates some compu-
326 tations that were made using a hypothetical dependence of $\mathcal{D}_{13|2}$. As can be
327 noted, a highly flexible modelling of the admissible set is possible.

328 This dependence structure corresponding to the last case listed in table 2 is
329 illustrated in figure 3. Since the parameter describing the dependence in $\mathcal{D}_{13|2}$
330 varies according to a trigonometric description, this set is not convex. This

Table 2: Results of the propagation of the interval uncertainty and admissible set in eq. (33) with $\theta_3^1(x_2) = (1 - \exp \frac{x_2}{\max(x_2)}) / (1 - \exp \frac{x_2}{\max(x_2)})$ and $\theta_3^2(\omega) = \sin(4*\omega - \pi/2), \omega = 0, \dots, 4*\pi$

$\theta = [\theta_1, \theta_2, \theta_3]$	\hat{x}	\hat{x}	y^I
$[0, 0, x_2]$	$[1, 2, 5]$	$[4, 6, 5]$	$[-8, 14]$
$[0.5, 0.5, x_2]$	$[1, 4, 4]$	$[4, 4, 4]$	$[-4, 8]$
$[0, 0, \theta_3^1(x_2)]$	$[1, 2, 5]$	$[4, 6, 4.9]$	$[-8, 14.2]$
$[0.5, 0.5, \theta_3^1(x_2)]$	$[1, 4, 4.279]$	$[4, 4, 3.721]$	$[-4.558, 8.558]$
$[0.75, 0.5, \theta_3^2(\omega)]$	$[1, 5.5, 5]$	$[3.62, 3.5, 3]$	$[-4.5, 6.68]$

331 visualization is obtained by propagating a Sobol Sequence containing $1 \cdot 10^{06}$
332 samples through the analytical function, discarding the values that do not com-
333 ply with the admissible set, and computing the alpha-shape representation of
334 the resulting data. This figure illustrates that also non-convex \mathcal{D} are obtainable
335 following the proposed approach. Note that such explicit computation is only
336 needed for visualization purposes, as the necessary computations of the indica-
337 tor functions are made for each step of an iteration of the optimization solvers.
338 Since this case study is only three-dimensional, no explicit difference between \mathfrak{D}
339 and \mathfrak{C} -vine pair constructions is included in the study, as both are in this case
340 analogous.

341 6. Case study 2: composite blade

342 6.1. Case introduction

343 The second case study concerns a finite element model of a long and slender
344 blade. The structure has a total length of 30 m and the width is 1 m at the widest
345 part. This blade is produced using a multilayer laminar composite material, with
346 deterministic ply material properties $E_1 = 231 \text{ GPa}$, $E_2 = 77 \text{ GPa}$, $\nu_{12} = 0.31$
347 and $G_{12} = G_{23} = G_{13} = 42.7 \text{ GPa}$. Different lay-ups are placed in the structure,
348 where close to the attachment of the blade (left-most), the lay-up is thicker as
349 compared to at the end-point (right-most). The blade consists of a composite
350 outside shell (top, leading edge, bottom, trailing edge), as well as two vertical

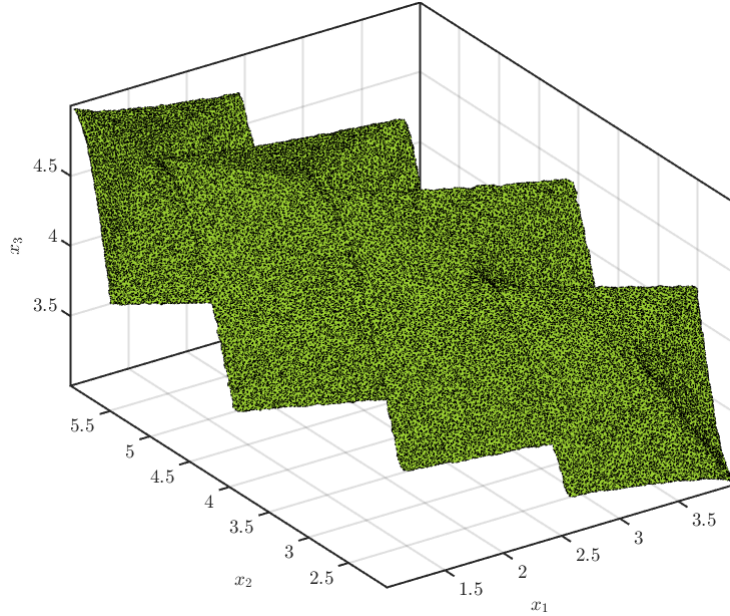


Figure 3: Illustration of the dependence structure of $\theta_3^2(\omega)$ used to model the dependence between 3 intervals. Comment: A Matlab live figure will be provided with the final version of the paper.

351 stiffening ribs in the centre. A total of 15 different composite lay-ups are present
 352 in the blade, which are summarized in table 3.

353 The dynamic behaviour of the structure is modelled using a Finite Element
 354 model containing 621 nodes, 606 bilinear shell elements, 573 rigid connections,
 355 10 concentrated masses and 132 rod elements. The left end of the composite
 356 blade is fixed rigidly. The finite element model of this structure is shown in
 357 figure 4.

358 The model is solved for its 10 first eigenmodes and corresponding resonance
 359 frequencies. Table 4 lists the result of the deterministic simulation. The effect
 360 of mode-crossover and -veering is accounted for by tracking the mode shapes
 361 via the modal assurance criterion.

362 The uncertainty the analyst has concerning the true values of the primary
 363 and secondary Young's modulus (E_1 and E_2), as well as the ply thickness in
 364 the red, yellow and blue areas indicated in figure 4 (t_1 , t_2 and t_3), is modelled

Table 3: Composite lay-up structure of the blade. Left means at $y = 0$ in figure 4 and the leading edge is depicted at the back side of figure 4.

Location	Lay-up (symmetrical)	thickness per layer (mm)
Top and bottom left	$+ - 45^0$	1.5 mm
leading edge left	$+ - 45^0$	1.5 mm
front-middle edge left	$+ - + - + - +45^0$	1.5 mm
back-middle vertical left	$+ - + - + - +45^0$	1.5 mm
trailing edge left	$+ - + - + - +45^0$	1.5 mm
Top and bottom middle	$+ - 45^0$	1.5 mm
leading edge middle	$+ - 45^0$	1.5 mm
front-middle edge middle	$+ - + - + - +45^0$	1.5 mm
back-middle vertical middle	$+ - + - + - +45^0$	1.5 mm
trailing edge middle	$+ - + - + - +45^0$	1.5 mm
Top and bottom right	$+ - 45^0$	1.5 mm
leading edge right	$+ - 45^0$	1.5 mm
front-middle edge right	$+ - + - + - +45^0$	1.5 mm
back-middle vertical right	$+ - + - + - +45^0$	1.5 mm
trailing edge right	$+ - + - + - +45^0$	1.5 mm

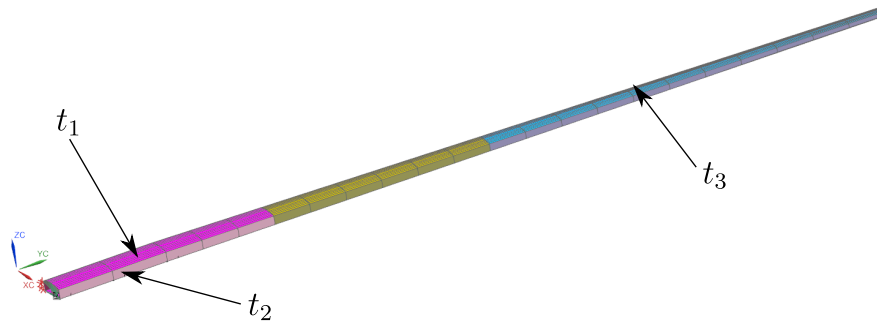


Figure 4: Finite element model of the composite blade

Table 4: Deterministic eigenmodes and -frequencies of the composite blade

Mode number	description	f
1	1 st vertical bending	0.79 Hz
2	1 st horizontal bending	2.07 Hz
3	2 nd vertical bending	3.11 Hz
4	3 th vertical bending	7.72 Hz
5	2 nd horizontal bending	8.67 Hz
6	4 th vertical bending	14.45 Hz
7	3 th horizontal bending	21.68 Hz
8	5 th vertical bending	23.84 Hz
9	1 st torsion	26.76 Hz
10	6 th vertical bending	35.01 Hz

365 as intervals. Specifically, these intervals are defined as $E_1 = [190, 200]$ *GPa*,
 366 $E_2 = [70, 77]$ *GPa*, $t_1 = [0.012, 0.015]$ *mm*, $t_2 = [0.015, 0.017]$ *mm* and $t_3 =$
 367 $[0.011, 0.018]$.

368 6.2. Artificial Neural Network meta-modelling

A single forward computation of the model takes about 20 seconds of wall-clock time on a high laptop equipped with 32 Gb or RAM and an Intel Core i7-7700HQ CPU @ 2.8 GHz. In case independent intervals are propagated, 32 deterministic model evaluations are needed. However, as is clear from table 1, this number can increase quickly when dependence is included in the analysis. Furthermore, since a comparison of the Extended Transformation Method with a Genetic Algorithm is performed, computational expenses can become high when such a global optimization is performed with the full FE model. Therefore, to limit the computational expense, a 4-layer sigmoid-symmetric Artificial Neural Network (ANN) with (5:10:1)-configuration is trained for each eigenfrequency and compiled to C++ for computational efficiency. The lay-out of the network is iteratively chosen where a maximum performance with a minimum

of hidden nodes is aimed at. Hereto, a training dataset containing 1750 samples is generated using Latin Hypercube Sampling between the interval bounds of the model uncertainty. Furthermore, a validation data set of 750 specimens was used to verify the accuracy of the trained ANN. To prevent over-training, Bayesian regulation back-propagation was used [42], which expresses the ANN model performance P as:

$$P = \frac{\xi}{d} \sum_{i=1}^d (y_{training,i} - y_{ANN,i})^2 + \frac{\chi}{d} \sum_{i=1}^d w_i^2 \quad (37)$$

369 with ξ and χ the regularisation parameters and $y_{training,i}$ and $y_{ANN,i}$ respec-
 370 tively the responses that are captured in the training data set, and the predicted
 371 responses of the ANN. When $\xi \gg \chi$, the network will drive the mean squared
 372 error to a lower value. Conversely, when $\chi \gg \xi$, the network weights and
 373 biases will be smaller as compared to a non-regularised performance function,
 374 forcing the network response to be smoother. Hence, the former case tends
 375 towards a perfect representation of the training data, albeit with the risk of
 376 performing bad on new data, whereas the latter aims at a better generalisa-
 377 tion performance of the ANN. Specifically, this training is performed following
 378 a Bayesian approach, where the weights w and biases b are modelled as ran-
 379 dom variables, and identified following a Bayesian approach that minimises P .
 380 The regularisation parameters ξ and χ are related to the variances of the ran-
 381 dom weights and biases, and are also found by performing Bayesian estimation
 382 [43, 44]. These computations are performed using the Neural Network toolbox
 383 in Matlab. The performance of the ANN on both the training and validation
 384 data set is shown 5 for each eigenfrequency. As may be noted, a highly per-
 385 forming set of meta-models is obtained, and hence, they can be used to make
 386 viable predictions about the model behaviour at strongly reduced cost.

387 6.3. \mathfrak{D} -vine decomposition

A first illustration of the admissible set decomposition follows the \mathfrak{D} -vine approach. This corresponds to the case where the analyst has direct knowledge about dependence between E_1^I, E_2^I on the one hand and t_1^I, t_2^I and t_3^I on the other

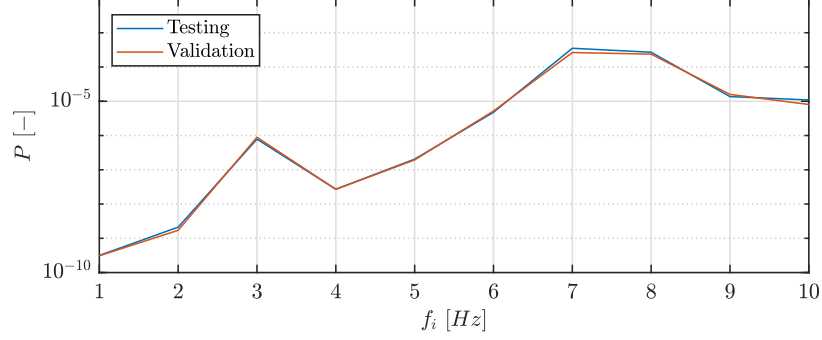


Figure 5: Performance of the ANN on the training and validation data set

hand. Specifically, the \mathcal{D} -vine decomposition of the admissible set of parameters $\mathcal{D}(E_1^I, E_2^I, t_1^I, t_2^I, t_3^I)$ can be written explicitly as:

$$\begin{aligned}
\mathcal{D}(E_1^I, E_2^I, t_1^I, t_2^I, t_3^I) = & E_1^I \times E_2^I \times t_1^I \times t_2^I \times t_3^I \cap \\
& \mathcal{D}_{12} \cap \mathcal{D}_{23} \cap \mathcal{D}_{34} \cap \mathcal{D}_{45} \cap \\
& \mathcal{D}_{13|2} \cap \mathcal{D}_{24|3} \cap \mathcal{D}_{35|4} \cap \\
& \mathcal{D}_{14|23} \cap \mathcal{D}_{25|34} \cap \\
& \mathcal{D}_{15|234}
\end{aligned} \tag{38}$$

388

When only pairwise dependence between E_1^I, E_2^I on the one hand and t_1^I, t_2^I

389 is considered, the different terms in eq. (38) are given in this case study by:

$$\mathcal{D}_{12} = \mathcal{H}(|E_2 + E_1 - 1| - \theta_1) \quad (39)$$

$$\mathcal{D}_{23} = E_2^I \times t_1^I \quad (40)$$

$$\mathcal{D}_{34} = \mathcal{H}(|t_1 - t_2| - \theta_2) \quad (41)$$

$$\mathcal{D}_{45} = \mathcal{H}(|t_2 - t_3| - \theta_3) \quad (42)$$

$$\mathcal{D}_{13|2} = E_{1|E_2}^I \times t_{1|E_2}^I \quad (43)$$

$$\mathcal{D}_{24|3} = E_{2|t_1}^I \times t_{2|t_1}^I \quad (44)$$

$$\mathcal{D}_{35|4} = t_{t_1 t_2}^I \times t_{t_3|t_2}^I \quad (45)$$

$$\mathcal{D}_{14|23} = E_{1|E_2 t_1}^I \times t_{2|E_2 t_1}^I \quad (46)$$

$$\mathcal{D}_{25|34} = E_{2|t_1 t_2}^I \times t_{3|t_1 t_2}^I \quad (47)$$

$$\mathcal{D}_{15|234} = E_{1|E_2 t_1 t_2}^I \times t_{3|E_2 t_1 t_2}^I \quad (48)$$

390 with θ_i a measure for the dependence between the interval parameters [9]. In
 391 this case study, $\boldsymbol{\theta} = [0.5; 0.9; 0.7]$. These values are chosen purely for illustrative
 392 purposes. The corresponding admissible sets correspond to the case where E_1
 393 and E_2 have a negative dependence and t_1 , t_2 and t_3 have a positive depen-
 394 dence. Physically, the former could be explained by unmodelled uncertainty
 395 on the fibre-matrix mixture ratio in the composite material, yielding a nega-
 396 tive dependence between these two Young's moduli. The positive dependence
 397 between the thickness values on the other hand can for instance originate from
 398 some systematic but unknown offset in the lay-up process. As can be noted, the
 399 higher order terms are not included, as they are all represented by a Cartesian
 400 product. Note than any kind of dependence structure can be applied for the bi-
 401 variate admissible sets. The result of propagating \mathcal{D} is compared to propagating
 402 a 5-dimensional hyper-cubic input set.

403 The cross-sections of this 5-dimensional convex dependence region are shown
 404 in figure 6. The blue area is the domain covered by the independent intervals,
 405 whereas the orange area corresponds to the admissible set that is defined. AS
 406 can be noted, the method allows for the independent modelling of the depen-

407 dence between the Young's moduli and the thickness values by selecting the
 408 appropriate decomposition structure and corresponding values.

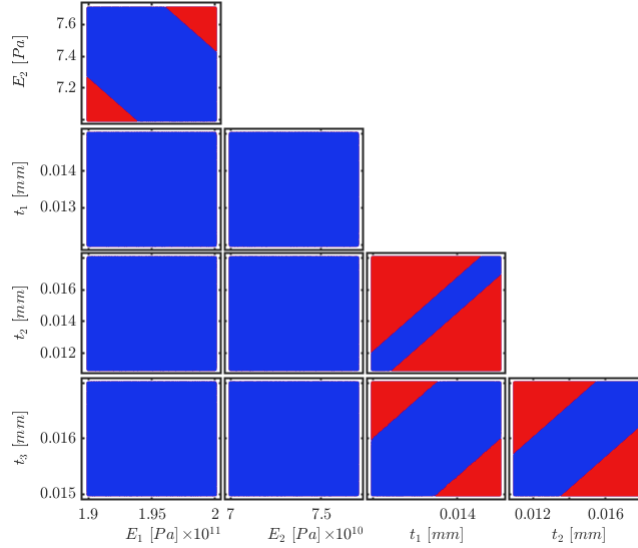


Figure 6: 2-dimensional intersections of the 5-dimensional admissible set \mathcal{D} . Red: hyper-cubic space covered by the independent intervals. Blue: intersections of the admissible set.

409 Based on this decomposed set, the optimisation problem that is introduced
 410 in eq. (24) is solved for the 10 first resonance frequencies of the composite blade.
 411 This is specifically obtained by means of a Genetic Algorithm that starts from an
 412 initial uniform distribution between the interval bounds consisting of 50 samples.
 413 An elite count of 3 was used, together with a forward migration factor of 0.2, a
 414 Gaussian mutation function and a cross-over fraction of 0.8. The algorithm is
 415 deemed to be converged when the improvement of the objective function over 50
 416 subsequent generations is smaller than $1 \cdot 10^6$. Such optimization is performed
 417 for each bound of each resonance frequency. Hence, 20 optimization procedures
 418 should be performed. On average, one call to the Genetic Algorithm solver
 419 requires $\mathcal{O}(10^4)$ deterministic function evaluations for this specific FE model.
 420 Making use of the ANN meta-models and parallel processing, this is well within

421 feasible computational cost.

422 The result of this optimization procedure is illustrated in figure 7. This
 423 figure shows two-dimensional cross-sections of the 10-dimensional result mani-
 424 fold, obtained by propagating 50000 Sobol samples from the dependent input
 425 parameters. As can be noted, when more dependence is included in the analy-
 426 sis, the solution manifold becomes smaller and smaller. Furthermore, also the
 427 dependence between the resonance frequencies is impacted.

428 The result of the optimization runs is illustrated in this figure as green
 429 crosses. As is clear, the bounded optimization problem yields the exact (hyper-
 430 cubic) bounds on the eigenfrequency.

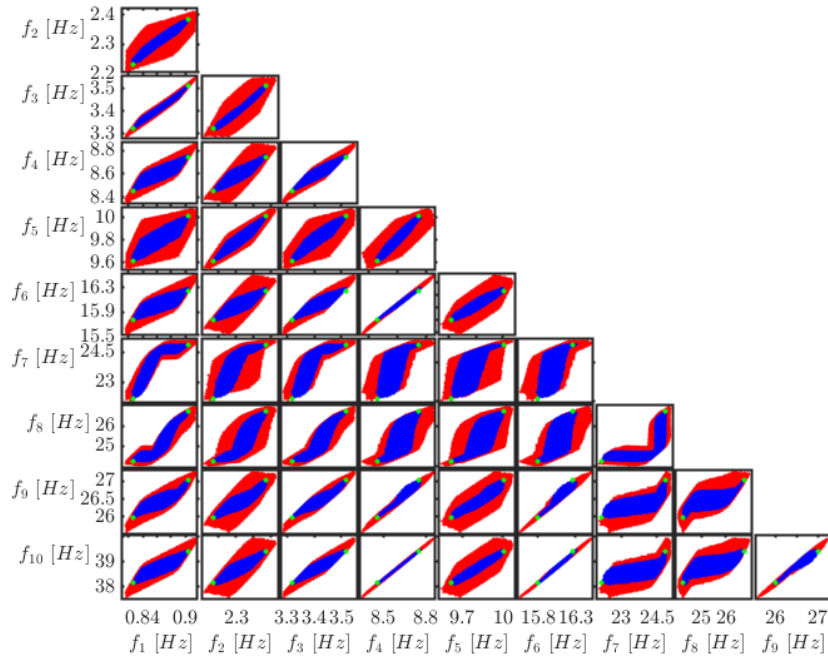


Figure 7: 2-dimensional intersections of the 10-dimensional eigenfrequency space. Red: result of propagating the independent intervals. Blue: result of propagating the dependent intervals via the admissible set \mathcal{D} with the Extended Transformation Method. Green dots: result of propagating the dependent intervals via the admissible set \mathcal{D} via Global Optimization.

431 The decomposition of \mathcal{D} according to a \mathcal{C} -vine decomposition is straightfor-
432 ward and can be performed in full analogy to the presented case studies.

433 **7. Conclusions**

434 This paper presents a flexible approach for the modelling of dependent in-
435 tervals for multivariate input spaces. Specifically, it is proposed to construct
436 the dependence structure in a similar approach to copula pair constructions,
437 yielding a limited set of 2-dimensional dependence functions. Also, the well-
438 known transformation method is extended to account for dependence between
439 multiple intervals. A first case study, where the developed method is applied to
440 an analytical function is included to illustrate the main ideas. Application of
441 the enriched transformation method indicates that by introducing dependence
442 between the model parameters, the width of the output interval is decreased
443 significantly. The second case study applies the methodology to a realistic finite
444 element model of a long, slender composite blade. Two different dependence
445 structures are propagated and it is shown that the method is well capable of
446 limiting the set of admissible parameter combinations, yielding tighter output
447 sets. However, the computational cost of propagating the dependent intervals,
448 both via global optimization as the enriched transformation method scales badly
449 with the dimension of the input space, but also with the nature of the depen-
450 dence. Application of surrogate modelling was used to alleviate this problem.

451 **Acknowledgements**

452 The authors would like to acknowledge the financial support of the Flemish
453 research foundation in the framework of the research project G0C2218N and
454 the post-doctoral grant 12P359N of Matthias Faes. The authors also would like
455 to thank the reviewers for the constructive criticism and remarks.

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