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Three step deep reactive ion etch for high density trench etching

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Abstract. A three step Deep Reactive Ion Etch (DRIE) process is developed to etch trenches of 10 μ m wide to a depth of 130 μ m into silicon with an etch rate of 2.5 μ m min⁻¹. The aim of this process is to obtain sidewalls with an angle close to 90°. The process allows the etching of multiple trenches with high aspect ratios that are closely placed together. A three step approach is used as opposed to the more conventional two step approach in an attempt to improve the etching selectivity with respect to the masking material. By doing so, a simple AZ6632 positive photoresist could be used instead of the more commonly used metal masks which are harder to remove afterwards. In order to develop this process, four parameters, which are the bias power, processing pressure, step times and number of cycles, are evaluated an optimized on a PlasmaPro 300 Cobra DRIE tool from Oxford Plasma Technology.

1. Introduction

Deep reactive ion etching (DRIE) is used to create deep, steep sided features in silicon wafers with aspect ratios (etch depth/feature width) beyond 10:1. The technique is developed and licensed by Robert Bosch GmbH [1] and relies on the repeated alternation of isotropic silicon etching and passivation steps to obtain anisotropic profiles. F-based plasmas such as SF_6 are generally used for fast isotropic silicon etching. whereas F-based inhibitor plasmas such as C_4F_8 are generally used to obtain directionality. Figure 1 shows the general process flow. Classically, the selective removal of the fluorcarbon and the isotropic etching is combined into one step: the etching step. However as indicated by others [2], a higher etch selectivity with respect to the masking material can be obtained by subdividing the etch step in two parts. The first part is then optimized towards selective removal of the fluorcarbon film deposited at the bottom of the trench, whereas the second part is optimized towards fast isotropic etching. This gives rise to a so called three step DRIE process. Such a process is a big advantage when used in combination with CMOS processing. Because of the higher etch selectivity with respect to the masking material, photoresists can now be used as masking material even for through wafer trenches and holes. This in contrast to the more conventional materials used for that, such as oxides or metals, which are harder to remove afterwards without damaging useful oxides or metals in the CMOS stack underneath.

The main considerations when developing a DRIE process include side-wall verticality, bottom roughness and etching rate of both silicon and masking material. All of these are affected by process parameters such as plasma power, pressures, gas flows, bias power, cycle times and substrate cooling. This is a wide set of processing parameters that are all interconnected and



Figure 1. DRIE process. (a)Isotropic silicon etch. (b)Fluorcarbon film deposition. (c)Selective fluorcarbon film removal. (d)Isotropic Silicon etch.

thus need careful optimization for each specific etching job. This paper will mainly focus on four of these parameters, which are bias power, processing pressure, step times and number of cycles. All the experiments are conducted on a PlasmaPro 300 Cobra DRIE tool from Oxford Plasma Technology.

2. Experimental details

For the experiments, 500 µm thick <100>boron doped Si-wafers with a resistivity of 10-20 Ω cm are used. These are spincoated with the positive photoresist AZ6632 at a speed of 2000 rpm for 30 s. The soft bake is conducted at 120 °C for 4.5 min. Before developing in an 4:1 diluted 351-solution, the resist is UV-exposed with a dose of 100 mJ cm⁻². The development is finished with a hard bake of 4.5 min at 125 °C. This is done in order to improve the etch resistivity of the resist during the DRIE processing. The actual patterns are parallel grooves with a length of 5000 µm, a width of 10 µm and a pitch of 18 µm. Grooves with equal length but smaller widths and pitches are also patterned and etched alongside but are not further discussed in this paper.

In order to save costs and reduce the etch mask variability of different experiments, only small pieces ($\sim 4 \text{ cm}^2$) of the patterned wafer are processed. This is done through manual diamond cleaving. However, a carrier substrate is still needed to properly clamp and cool the pieces in the DRIE tool. The carrier also functions as a protection for the bottom electrode. In this work SiOx was used as carrier and reused across the different experiments. Fomblin[®]-oil or thermal grease was used to temporarily bond the two.

A three step process provided by the DRIE tool manufacturer was used as a starting point. The effect of parameter changes on the output will be discussed next. After DRIE processing, samples were again cleaved with a diamond to inspect the cross section with a FEI XL30 secondary ion emission microscope. Photoresist thicknesses before and after processing were measured with a Dektak[®]XL stylus profilometer.

3. Results and discussion

The initial parameters of the three step process are given in table 1. Due to the addition of the extra breakthrough step as compared to the more conventional two step DRIE process, it is now possible to alter process parameters after fluorcarbon removal at the bottom of the trench. Main parameters altered here are: SF₆-flow, pressure and bias power. After 100 cycles, the process of table 1 resulted in a 68 µm deep trench with a Si to mask etch selectivity of 52:1. The profile is severely negative tapered with a sidewall angle of 91.9°. This limits the usability of the process if one wants to etch trenches with a small pitch, especially if the trenches needs to be very deep. Therefore the effect of several parameters is studied in order to straighten the trench profile without compromising on the etch selectivity in the existing three step process.

Step	Time (s)	$\frac{\mathrm{SF}_{6}}{(\mathrm{sccm})}$	C_4F_8 (sccm)	Pressure (mbar)	Plasma power (W)	Bias power (W)
Deposition	2	10	200	0.033	2500	0
Breakthrough	2	200	10	0.040	2000	35
Etch	2	400	10	0.093	2500	0

Table 1. Three step process parameters and their initial values.

3.1. Bias power

The first parameter under study is the bias power. According to [3], sidewall angles become more positive tapered by lowering the bias power in the etch step of a two step process. As can be seen in figure 2, similar results are obtained in this paper with the three step process by lowering the bias power during the breakthrough. An interesting side effect is the increase of the etch selectivity with respect to the resist mask. Which confirms that resist mask erosion is mainly caused by ionic impact. Switching off the bias power after fluorcarbon removal, as is done in a three step process, is thus a viable route to enhance the Si to resist etch selectivity.



Figure 2. Effect of bias power during the breakthrough on the Si to resist etch selectivity and sidewall angle.

One drawback however of decreasing the breakthrough power is the reduced overall etch rate, which dropped from $6.8 \,\mu\mathrm{m}\,\mathrm{min}^{-1}$ at $35 \,\mathrm{W}$ to $5.9 \,\mu\mathrm{m}\,\mathrm{min}^{-1}$ at $9 \,\mathrm{W}$. This is due to the reduced contribution of the breakthrough step to the actual silicon etching. Similar results should thus be found by keeping the bias power constant and reducing the breakthrough step time. Unfortunately a 2 s step time is already close to the minimal switching time of the machine, which is limited by the response time of the mass flow controllers. Another limiting factor in this experiment was the accuracy of the automatic matching unit. If bias power was lowered to $4 \,\mathrm{W}$, matching became impossible, resulting in total power reflection and almost no silicon etching.

3.2. Breakthrough pressure

With bias power adjusted to 9 W the effect of breakthrough pressure is investigated. Lowering the pressure from 40 µbar to 30 µbar further improved the sidewall angle to 90.4°. This is most probably due to the longer mean free path of SF₆-ions which in term leads to a lower ion dispersion in the dark region between the substrate and the plasma [2]. Thus causing less etching of the sidewall polymer. However both selectivity and overall etch rate dropped to 84.6:1 and $5.5 \,\mu m s^{-1}$ respectively. Due to the limited pump capacity and the chosen flow rates, the minimal attainable pressure is 25 µbar. Yet this pressure is never experimented with since the pressure in the subsequent etching step, which is 3.7 times higher, was already difficult to reach in the 2s time slot.

3.3. Deposition time

A natural parameter to tune in order to change the sidewall angle, is the deposition step time. The longer this step lasts, the more polymer is deposited and the harder it becomes to remove it from the sidewalls in the subsequent step. As a consequence more positive tapered slopes are obtained [4]. Doubling the deposition time to 4s resulted in a perfect sidwall slope of 90° and a 1.4 times better conservation of the mask material. But due to overpassivation, the etch rate severely dropped to $2.25 \,\mu m \, s^{-1}$. As stated before, the sidewall angle of deep trenches is the main focus of this research. Therefore further optimization of the deposition time is omitted at this point. But it is important to mention that reducing the deposition time to overcome overpassivation will lead to higher overall etch rates, without affecting both sidewall angle and mask removal rate. Testing the process developed so far to check if the observations still hold with more cycles is now more interesting in achieving deep straight walled trenches.

3.4. Number of cycles

By doubling the number of cycles to 200 and keeping all the other parameters the same, trenches were, as expected, twice as deep. However the sidewall angle slightly increased to 90.4°. This is due to an effect called imaging force. As explained in [2] and [5] imaging force is the deflection of ions entering a trench towards the sidewalls due to the negative potential of these conducting silicon sidewalls with respect to the plasma glow. As trenches become deeper, more deflection will occur which in term leads to the observed profile. As the number of cycles is increased



Figure 3. Etching result after (a)200 cycles and (b)400 cycles.

even further to 400 cycles the observed profile changes completely. As can be seen in figure 3: sidewalls become positive tapered with an angle of 89.1° and grassing is observed at the bottom of the trench. The formation of the grass and the positive sloped sidewalls are due to an imbalance in polymer removal and deposition [6]. Too much polymer is deposited with respect to breakthrough and etch step. The reason why it only appears in deeper trenches is because the polymer removal at the bottom becomes less effective at higher aspect ratios. This is a consequence of imaging forces and dispersion of ions due to collisions in the plasma glow [2], basically the same mechanisms that are thought to cause the aspect ratio dependent etching (ARDE) [2].





To prevent grassing from occurring, more directional ions during the breakthrough are thus needed. Since pressure is already minimized, bias power should therefore increase. However an increase in bias power also leads to faster mask removal and worse selectivity as indicated in figure 2. Because the higher bias power is only needed at high aspect ratios one can first etch trenches with a low bias power and later on switch to a higher bias power. The result of this approach, where the first 200 cycles are etched at 9W and the subsequent 200 cycles at 14 W, is shown in figure 4. These trenches have sidewall angles of 89.7° and are 130 μ m deep. The sidewall damage seen at 80% of the trench depth is most probably due to mask erosion as explained in [7].

Conclusion

By analysing the effect of bias power, breakthrough pressure, deposition time and number of cycles on etch characteristics in a three step DRIE process. A recipe is developed to etch 130 μ m deep trenches in silicon with a width of 10 μ m. The sidewalls are almost vertical with an angle of 89.7°, which is a strict requirement for high density deep trench etching. Excellent silicon to photoresist etch selectivity of 50:1 is achieved due to limited usage of high energy ions during breakthrough. This obviates the use of metal or oxide masks for through wafer etching applications such as: comb drives, springs and through wafer vias. Which is a big advantage when combined with CMOS processing. Currently the proposed 400 cycle process with an etch rate of 2.45 μ m min⁻¹ is used to etch mechanical structures with thicknesses starting from 100 μ m.

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References

- [1] Robert Bosch GmbH 1994 Pat. 4,855,017 and 4,784,720 (USA) and 4241045C1 Germany
- [2] Jansen H V, De Boer M J, Unnikrishnan S, Louwerse M C and Elwenspoek M C 2009 J. Micormech. Microeng. 19 033001-41
- [3] Ayón A A, Braff R, Lin C C, Sawin H H and Schmidt M A 1999 J. Electrochem. Soc. 146 339-49
- [4] Abdolvand R and Ayazi F 2008 Sens. Actuators A 144 109-16
- [5] Elwenspoek M and Jansen H V 2004 Silicon Micromachining (Cambridge: Cambridge University Press)
- [6] Ayón A A, Chen S, Lohner A, Spearing S M, Sawin H H and Schmidt M A 1998 Proc. Material Research Society (Cambridge) vol 546 Heuer A H and Jacobs S J (Cambridge: Material Research Society) p51
- [7] Meng L and Yan J 2015 J. Micormech. Microeng. 25 035024-32