

Co-W nanocrystalline electrodeposits as barrier for interconnects

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Abstract This study was performed in order to investigate a possibility to obtain Co-W microbumps via electrochemical routes, because this alloy recently has gained attraction as a novel barrier against copper diffusion. In order to be applied in flip-chip technology, barrier layers should be void-free and uniformly deposited on the entire area of a die to ensure high reliability and high performance of wafer bump-solder interface. To meet these requirements, a set of potentiostatic and galvanostatic electrodeposition was carried out from a citrate electrolyte, at pH 5 and at room temperature. The tests done confirm that void-free Co-W bumps with a uniform tungsten content along the bump can be obtained by potentiostatic and galvanostatic electrodeposition. Successful electrodeposition of Cu/Co-W/Sn layers with good adhesion between them and uniformity on the entire array of bumps also was obtained. The XPS data confirm that electrodeposited Co-W layers can act as a good barrier between Sn and Cu.

Keywords Cobalt–tungsten alloy · Electrodeposition · Diffusion barrier · Flip-chip technology

Introduction

The fabrication of microstructures with a relatively large thickness has attracted attention due to important applications as: Information and Communication Technology (ICT) (e.g., components in microelectromechanical systems (MEMS) and interconnect vias), chemical engineering, automation and robotics, environmental engineering, and medical technology [1–3]. Such microstructures can be obtained by electrodeposition processes like electrochemical through-mask plating, through-silicon vias (TSV) electrodeposition, which offer a high precision and the possibility to achieve features with high aspect ratios at different length scales.

Short and reliable interconnections become more and more critical for packaging of both mixed-signal wireless modules and digital processors. In these cases, thinner packages with embedded actives begin to drive the demand for interconnections having less than 30 μm pitch and 10 μm height [4, 5]. For high-speed computing, the I/O density determines the highest aggregate system performance both in multi-core processors and 3D ICs. The success of flip-chip technology resulted in several advances in the solder bump interconnections. With higher power densities, the electrical current through the bump increases, resulting in a higher bump temperature that accelerates electromigration and thermomigration [6]. However, even for the Cu bump, electromigration failures are seen at the bump/solder interface due to voids that occur between the Cu- and Sn-containing IMCs (Inter Metallic Compounds) and the solder [7].

Thus, in order to increase the electromigration resistance, a diffusion-barrier layer is inserted between the Cu bump and the solder joint, e.g., Co [3]. Cobalt has a much lower solid-

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state diffusion coefficient than W. Tungsten being a refractory metal also possesses superior diffusion barrier capabilities at higher temperatures. The incorporation of W into Co clogs up the grain boundaries [3]. Therefore, it can be anticipated that codeposition of Co with W should possess a good barrier capabilities. Indeed, Co-W alloys are being currently explored recently as advanced diffusion barriers to increase the electromigration resistance [8–10]. The recent research on Co-W alloys implies PVD- and CVD-based techniques that are more sophisticated and expensive than electrodeposition. Moreover, CVD requires specific compounds, like carbonyls (poisonous), making those processes less attractive. Whereas electrodeposition is less complicated, less expensive, does not require expensive equipment, and allows easy tuning of properties of the alloy.

The criteria for successful electrodeposition in the recesses are the void-free filling of them and a reduced deposition times [11–13]. Mass transport is of critical importance during electroforming, because the different concentration profiles result in gaps of different lateral sizes. The investigation of current distribution and deposit shape-change during electrodeposition into recesses needs to be performed. Different scales must be taken into account with respect to the current density distribution and mass transport [14]. Methods to increase mass-transport of the deposited metal ions include ultrasonic agitation [15], increasing the temperature of the electrolyte [16], and pulse-electroplating mode [17]. With increasing structural heights and decreasing in lateral dimensions, a lower contribution of convection to mass transport can be observed [18]. A clear influence of the aspect ratio on mass transfer was observed. Moreover, in order to entirely fill up the micro-sized patterns, the grain size of the electrodepositing metal or alloy should be small, i.e., electrodeposits have to be of nanocrystalline dimensions. Thus, in this paper, we will focus (i) on the adapting the gained experience on electrodeposition of tungsten alloys on flat surfaces [19–21] for obtaining void-free Co-W bumps as a promising diffusion-barrier layer for interconnects and (ii) on electrodeposition of tri-layered bumps as Cu/Co-W/Sn having good adhesion between layers and uniformity on the entire array of bumps on the coupon scale.

Experimental

Co alloyed with tungsten is usually obtained from water-based complex electrolytes: pyrophosphatic, glutamate-based, and so on [22–24]. In this work, a citrate-based Co/W electrolyte is used [19] with the following composition: 0.2 M $\text{CoSO}_4 \cdot 7\text{H}_2\text{O}$ + 0.2 M $\text{Na}_2\text{WO}_4 \cdot 2\text{H}_2\text{O}$ + 0.25 M $\text{Na}_3\text{C}_6\text{H}_5\text{O}_7 \cdot 2\text{H}_2\text{O}$ + 0.04 M $\text{C}_6\text{H}_8\text{O}_7$ + 0.65 M H_3BO_3 . The pH of the solution was adjusted with concentrated sulfuric acid to a value of 5.0. In every process involving the reduction

of a Co compound, one of the most important side reactions is hydrogen evolution. As H_2 evolves nearby the electrode and pH in that particular layer increases, favoring the formation of intermediate Co hydroxo-compounds. Therefore, the buffering agents are added to the electrolytes, in our case boric acid [25]. Substrates for deposition were of high purity silicon coated by PVD with 150 nm pure Cu. The photoresist itself has a special pattern formed by lithography in it—round shaped pits (Fig. 1a), reaching down to the Cu seed layer and exposing it. Each pit has a diameter of 15 μm and is 12 μm deep (Fig. 1b).

The substrate was cut to form coupons of the total working area for electrodeposition 0.01137 cm^2 . Before electrodeposition, every sample was washed and activated for 1 min with diluted sulfuric acid (1:100) containing a commercial wetting agent. The electrochemical system was a typical three electrode setup with an AgCl electrode in a saturated KCl solution as the reference electrode and a platinum mesh as the counter electrode. All values of electrode potentials are presented against that reference electrode. Electrodeposition was carried out with AUTOLAB302 operated with GPES and NOVA software. After electrodeposition onto the wafer piece, the photoresist was washed off in an ultrasonic bath with acetone and ethanol. The resulting bumps were investigated by SEM, FIB, and EDX.

The resistivity of electrodeposited Co-W layers was evaluated using the four-point van der Pauw resistivity

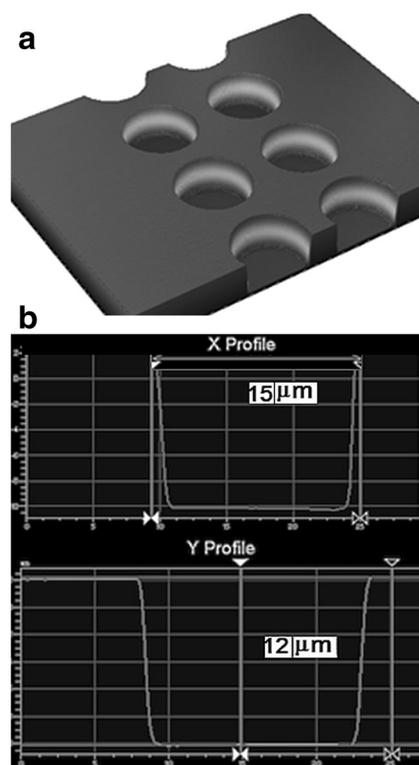


Fig. 1 Images (a) of a fragment of array of pits on the wafer (b) and a depth profile of the pit (c)

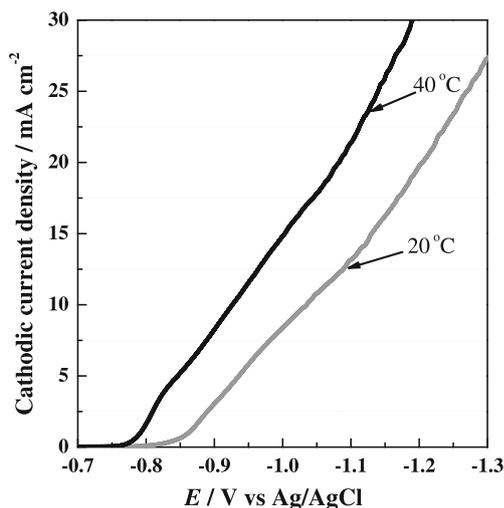


Fig. 2 Cathodic potentiodynamic polarization curves obtained on the planar electrodes without solution agitation. Solution; 0.2 M $\text{CoSO}_4 \cdot 7\text{H}_2\text{O}$ + 0.2 M $\text{Na}_2\text{WO}_4 \cdot 2\text{H}_2\text{O}$ + 0.25 M $\text{Na}_3\text{C}_6\text{H}_5\text{O}_7 \cdot 2\text{H}_2\text{O}$ + 0.04 M $\text{C}_6\text{H}_8\text{O}_7$ + 0.65 M H_3BO_3 adjusted to pH 5.0, potential scan rate of 10 mV s^{-1}

measurement method on plane wafers coated with a sputtered Cu layer (thickness; 500 nm). The resistivity of the Cu layer was measured, and then the required Co-W layer was electrodeposited. In this case, the total resistivity of the layers is represented as an in parallel connected resistivity of Cu and Co-W layers.

The barrier properties of Co-W layer were evaluated by elemental depth profiling of as-deposited and annealed samples. Samples annealing was carried in a tube furnace with argon flow at temperature $250 \pm 0.5 \text{ }^\circ\text{C}$ for 3 and 30 min. Depth profiling was done using X-ray photoelectron

spectroscopy (XPS, ULVAC-PHI Versaprobe). Cu 2p, Co 2p, W 4f, and Sn 3d spectra were obtained using alternating sputtering with Ar ion gun (acceleration voltage of 3 kV, sputtering raster $2 \times 2 \text{ mm}$, excentric rotation) and XPS analysis using focused monochromated Al K_α radiation (energy increment of 0.2 eV and pass energy of 23.5 eV). The obtained XPS data reduction (fitting, Target Factor Analysis) and analysis were performed using the Multipak software.

Results and discussion

Electrodeposition of Co-W into recesses

Prior to the electrodeposition of Co-W in the recesses, the compatibility of photoresist with solution was checked. The solution selected has already been investigated for Co-W electrodeposition on flat copper surfaces [21], at $60 \text{ }^\circ\text{C}$ and pH 6.7. The results showed that the photoresist did not withstand elevated temperatures and high pH values: all attempts to electrodeposit under such conditions resulted in a badly damaged photoresist. It was found that the photoresist can be used only at pH 5 and at room temperature, so a reasonable compatibility of the photoresist with the solution used for Co-W electrodeposition in the recesses was achieved. In order to estimate the electrodeposition potentials that can be used for Co-W electrodeposition, potentiodynamic polarization curves were recorded at pH 5 (Fig. 2).

Different potentials were applied in order to find the best conditions to deposit single-layered microbumps of Co-W alloys. The successful deposition was carried out at $20 \text{ }^\circ\text{C}$ at

Fig. 3 SEM images of Co-W electrodeposits obtained under potentiostatic electrodeposition into micro-recesses at room temperature. Deposition potentials; -0.87 V (a, d), -0.97 V (b, e), -1.07 V (c, f)

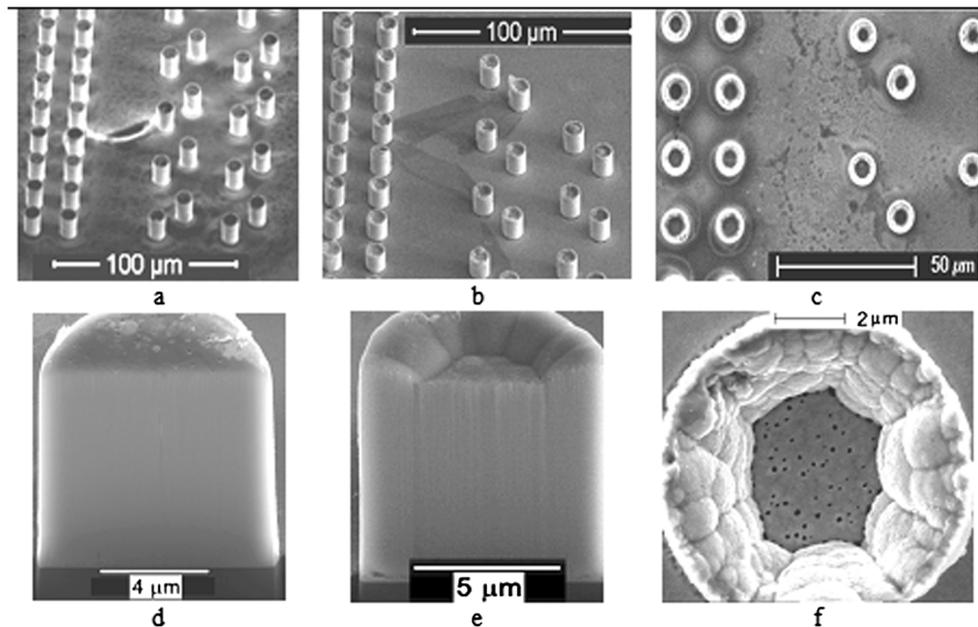
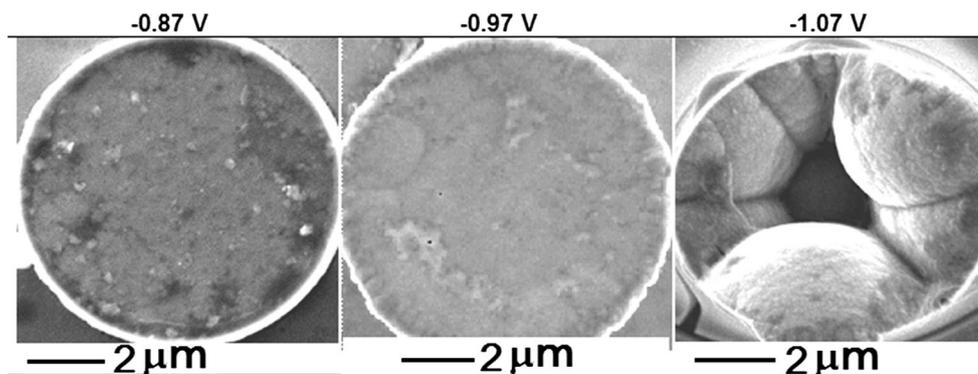


Fig 4 Co-W alloy electrodeposits into micro-recesses obtained at the potentiostatic mode at room temperature in the presence of stirring



a potential of -0.87 V vs. Ag/AgCl. Surface morphology of the electrodeposits obtained under these conditions is shown in Fig. 3. The electrodeposition took place inside the recesses with no visual damages of the photoresist. After the photoresist had been etched away with acetone, an excellent uniformity of the deposition was revealed, as shown in Fig. 3a. In order to find out whether the electrodeposit was void-free or not, cross sectional views were made by focused ion beam. In this case, the electrodeposit is fully dense, without any void inside as shown in Fig. 3d. The chemical composition of obtained Co-W deposit was analyzed along the microbumps, and for electrodeposited at the optimum potential of -0.87 V vs. Ag/AgCl, the tungsten content was 3.4 ± 1 at.%. Even at this small amount of tungsten the Co-W alloys are nanocrystalline [19], which caused a uniform filling of micro-recesses. In order to increase the rate of deposition, higher potentials were applied. However, as discussed in the introduction, the current distribution inside the recess may be not uniform: higher current at the edges of the recess compared to the center. Thus, the Co-W deposition occurs faster at the edge, as shown in Fig. 3b–f. The difference in height from edge to center was measured by a white light interferometer: $1 \mu\text{m}$ on average, at -0.97 V vs. Ag/AgCl; and at -1.07 V vs. Ag/AgCl, it is $2 \mu\text{m}$ on average for a bump height of $7 \mu\text{m}$.

In order to improve the mass transport conditions, stirring with a magnetic bar was used, and the entire uniformity was improved (Fig. 4). In this case, a good quality electrodeposit can be obtained also at more negative potentials, e.g., at -0.97 V vs. Ag/AgCl.

From the industrial point of view, the galvanostatic mode for electrodeposition is preferential over potentiostatic mode. In order to find the best galvanostatic conditions for Co-W deposition, several experiments were performed at $10 \div 35 \text{ mA cm}^{-2}$ cathodic current densities with 5 mA cm^{-2} increments and different stirring rates ($100\text{--}300$ rpm) in order to achieve the similar values of Co-W deposition potential. The changes in the Co-W deposition potential during electrodeposition at current densities applied under a 300 rpm stirring rate are shown in Fig. 5. Some examples of the obtained deposits are given in Table 1. Stirring improves the uniformity and

greatly increases the overall quality of deposits; optimal conditions were determined as the 30 mA cm^{-2} current density and 300 rpm rotation with similar tungsten content as during potentiostatic deposition.

At higher current densities, such as 35 mA cm^{-2} , hydrogen evolution becomes more pronounced, and it results in a lower overall uniformity (Fig. 6a) and sometimes even damages the bumps.

Resistivity of electrodeposited Co-W alloy

The electrodeposits serving as barrier layer should possess reasonable resistivity (ρ). In the case of solid solution alloys, ρ is described by Nordheim's rule:

$$\rho = X_A \rho_A + X_B \rho_B + C X_A X_B$$

where X_A and X_B are atomic fractions of alloy components A and B, respectively, ρ_A and ρ_B are the resistivity of the pure component A and B, respectively; C is a constant.

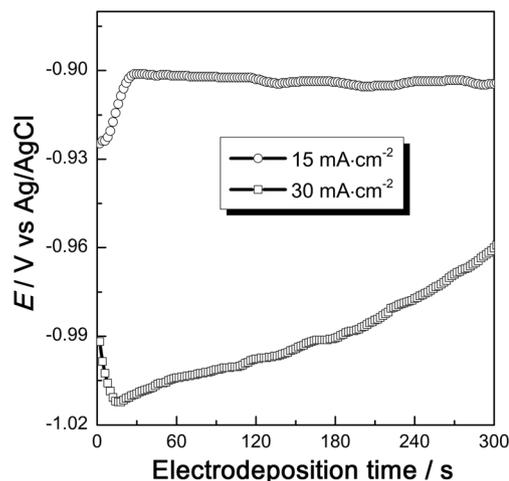
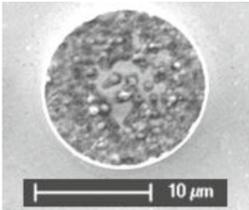
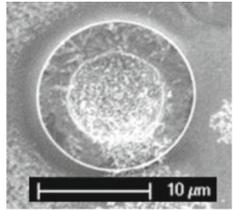
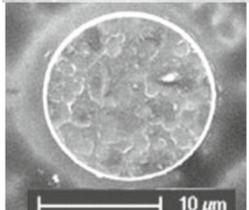
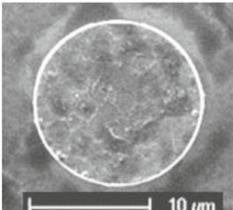
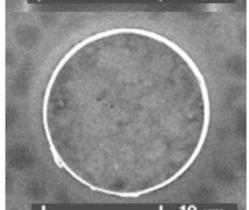
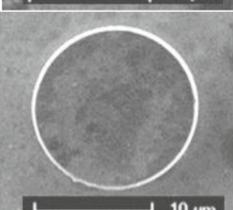
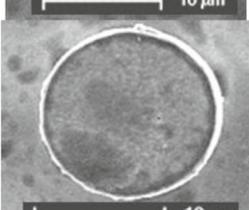
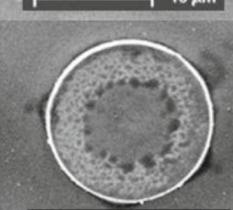
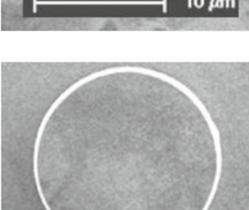
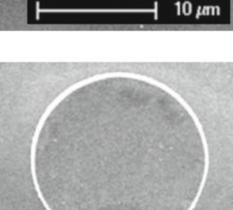


Fig. 5 Co-W deposition potential as a function of electrodeposition time at current densities 15 and 30 mA cm^{-2} at 20 °C and stirring rate of 300 rpm

Table 1 Typical SEM images of galvanostatically deposited Co-W bumps (*bottom* and *top* refer to bumps located at bottom and top part of the electrolytic cell, index “s” means the presence of stirring)

mA/cm^2	Bottom	Top	Growth rate, nm/min
-10			360
-20			320
-30			480
-35			580
-30 ^s			480

This equation evidently shows that the resistivity of alloy increases with the content of the component with higher resistivity in a non-linear way. Moreover, as grain size approaches the electrons mean free path, interconnect resistivity dramatically increases due to a higher resistivity contribution from surfaces and sidewalls [26].

The electrodeposited Co-W layer (3.5 at.% of W) possesses a resistivity dependent on the thickness of the electrodeposits, namely $24 \cdot 10^{-8} \Omega \text{ m}$ for $0.5 \mu\text{m}$ and $45 \cdot 10^{-8} \Omega \text{ m}$ for $2 \mu\text{m}$. The obtained values are similar to those obtained for electroless deposited barrier layers of Co-W-P alloys (2 wt.% W and 11 wt.% P): $28\text{--}32 \cdot 10^{-8} \Omega \text{ m}$ [27].

Deposition of multi-layered bumps

After determining the best conditions for Co-W alloys deposition into micro-recesses, the electrodeposition of multi-layered structures of Cu/Co-W and then tri-layered bumps consisting of Cu/Co-W/Sn were investigated, which actually acts as an interconnect meant to serve in microelectronic devices. The Co-W layer deposited between Cu and Sn layers acts as a barrier layer, suppressing electro-migration and diffusion of both Cu and Sn. In order to check the adhesion between the additional electrodeposited layer of Cu and Co-W alloy, the two-layered bumps were studied

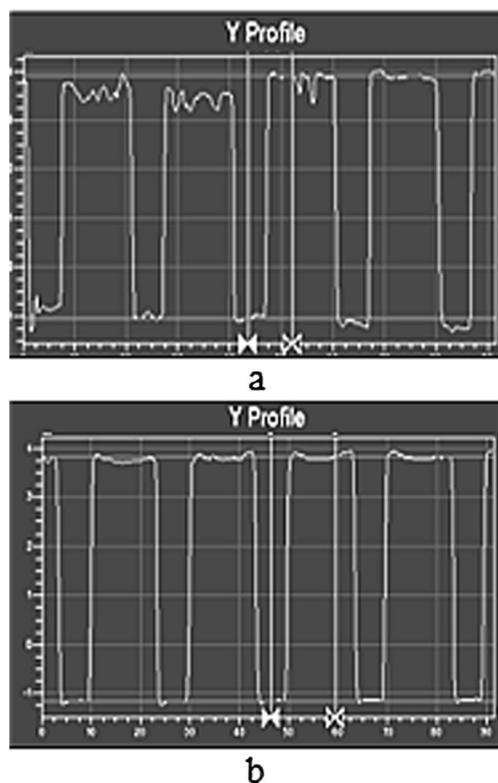
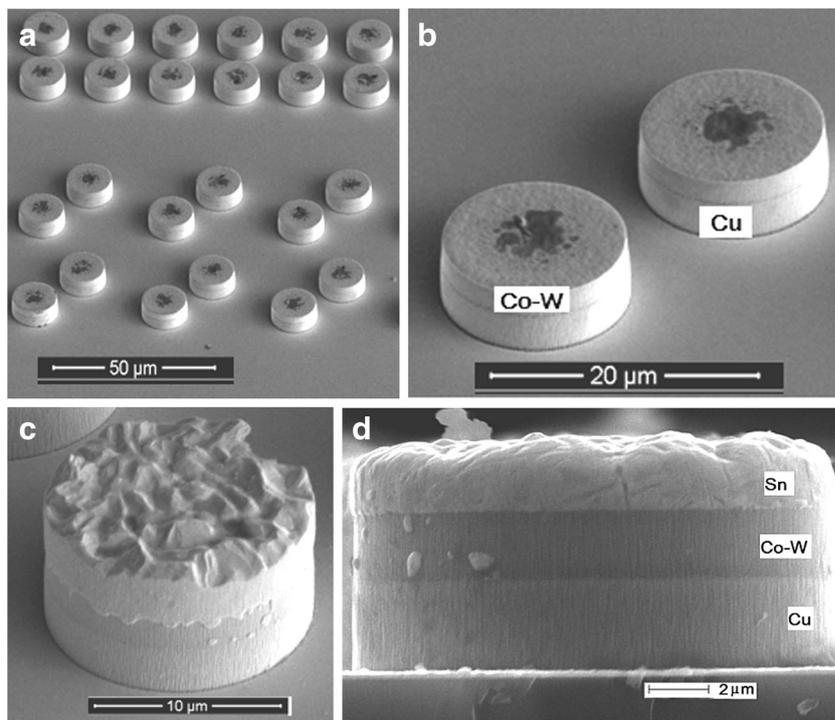


Fig. 6 Depth profiles of the Co-W deposits obtained at 35 mA cm^{-2} (a) and 30 mA cm^{-2} (b)

first, namely, Cu/Co-W. To do that, a 3- μm copper layer was electrodeposited onto wafer.

Fig. 7 Array of deposited double layered Cu/Co-W bumps (a, b) and triple layered bumps (c, d)

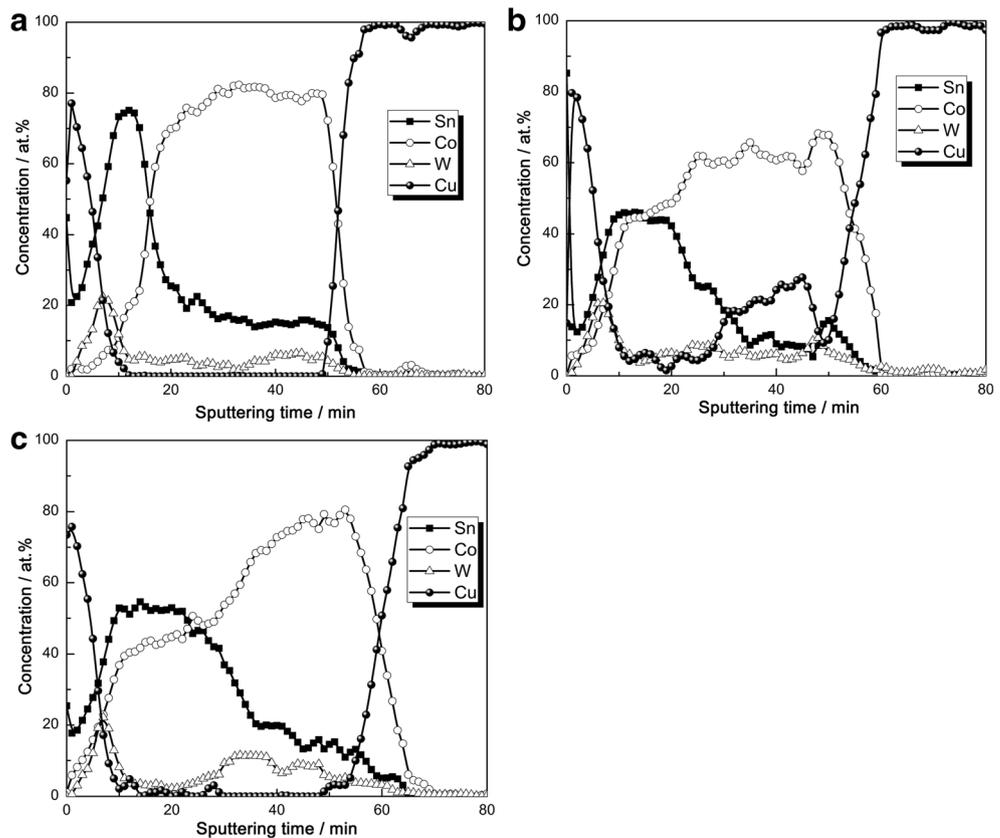


A copper plating solution containing 75 g l^{-1} of $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$ + 100 ml l^{-1} of H_2SO_4 + 2.5 ml l^{-1} of a commercial gleam additive (Cu Gleam PC, DOW) was used. The optimal current density for Cu electrodeposition from this solution was 20 mA cm^{-2} . Subsequently, the sample was transferred to another plating bath for the electrodeposition of $2 \mu\text{m}$ of Co-W under determined optimal conditions. FIB and SEM investigations showed a perfect uniformity and no internal cracks or delamination (Fig. 7a, b). Dark spots on these figures appeared probably due to the photoresist sticking to the bump sidewalls, after its removal in the ultrasonic bath. After getting evidence that the adhesion and uniformity between the Cu/Co-W layers in the bumps were good, the deposition of tri-layered coatings was carried out. The top layer was tin deposited from a commercial tin plating solution at 40 mA cm^{-2} (methanesulphonic acid-based, DOW, Solderon BP Sn-1000). The deposition parameters of Cu and Co-W were the same as for the double-layered bumps deposition. In that way, a successful process for tri-layered bump deposition was achieved: without internal cracks, delamination, or any other unwanted artefacts visible on FIB cross sections or SEM images (Fig. 7c, d).

Barrier properties of Co-W layer

The role of Co-W alloy as barrier layer is to prevent the diffusion of Sn from the top to the bottom of the Cu layer during soldering. The intermediate Co-W alloy consisting of 3–4 at.% W is a solid solution of the components [21].

Fig. 8 XPS profiles of as-deposited (a), heat treated at 3 min (b), and 30 min (c) tri-layered bumps



Therefore, we assume that solubility of Sn in this Co-W alloy and Co in Sn should be the same as in the case of pure Co. After Sn is heated at 250 °C, the solubility of Co in Sn at the Sn/Co boundary is as low as 0.04 wt.% and according to Sn-Co phase diagram possible intermetallic phases are CoSn, CoSn₂, and CoSn₃ [28]. The equilibrium between solid phases of α -Co₃Sn₂, β -Co₃Sn₂ should exist in the deeper layers at this temperature. If the resulting barrier layer is thick enough, the diffusion of Sn into the Cu layer during soldering is neglectable.

The diffusion of Sn into the Cu layer was evaluated experimentally by XPS depth profiling (Fig. 8). After deposition (Fig. 8a), some overlapping of the layers is present; however, relatively clear boundaries exist. The existing overlapping can be explained by several factors, such as the used X-ray beam size is approximately two times larger than the tri-layered bumps diameter. This helps to maintain the bump in the analysis field during eucentric rotation but at the same time a larger beam size results in the detection of photoelectrons originated not only from the selected bump but also from its surroundings. As it was discussed earlier, bumps are deposited onto Si covered by thin Cu layer. The latter Cu layer is responsible for the initial increase of the Cu concentration in Fig. 8a, b, and c (signal from Si does not appear in Fig. 8 because it was intentionally excluded from the figure). During sputtering, the ion beam is at a 45° angle to the surface normal

and for the bumps this means that there is a slightly not uniform sputtering from the center of the bump and from its edges. It is assumed that the latter effect is mostly responsible for the visible strong overlap of Sn and Co. Finally, in as-deposited bumps the occurrence of Sn diffusion into Cu can also be neglected.

After annealing at 250 °C for 3 and 30 min (Fig. 8a, b, respectively), a stronger overlapping of Sn and Co is observed. Therefore, it is assumed that during annealing a significant diffusion of Sn into Co takes place. In the overlapped region, the concentration ratio between Sn and Co is close to unity, and this indicates the formation of a stoichiometric CoSn alloy. Nevertheless, it is important to notice that despite the significant diffusion of Sn into the Co-W layer, Sn does not diffuse into Cu. This observation confirms that Co-W can be used as an effective diffusion barrier in the investigated tri-layered Sn/Co-W/Cu bumps.

Conclusions

In this study, Co-W alloys co-deposition in recesses was produced by potentiostatic and galvanostatic modes from a citrate electrolyte on a patterned wafer. Morphology and composition of the depositions were characterized. It was found that Co-W void-free microbumps can only be electrodeposited

at pH 5 and at room temperature because electrodeposition at higher pH or temperature causes the damage of the photoresist and yields non-uniform filling of recesses. The electrodeposition under stirring can essentially improve the overall uniformity and flatness of the deposited array, which is very important for future applications of Co-W layers into interconnects. High quality arrays of Co-W alloys electrodeposits were achieved under both potentiostatic and galvanostatic conditions. The resistivity of the obtained Co-W barrier layer depends on the thickness of the electrodeposits. It was $24 \cdot 10^{-8} \Omega \text{ m}$ for $0.5 \mu\text{m}$ and $45 \cdot 10^{-8} \Omega \text{ m}$ for $2 \mu\text{m}$, and these values are close to base materials used as barrier material. A successful processing of the Cu/Co-W/Sn tri-layered bump deposition was achieved without internal cracks, delamination, or any other unwanted artefacts. A Co-W alloy layer $2 \mu\text{m}$ thick was shown to act as a barrier layer because in as-deposited bumps and after heating at $250 \text{ }^\circ\text{C}$, the Sn diffusion into Cu can be neglected.

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